

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

C/SF
 File
 C-122 file

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 12-19-80	
Company HUSKY OIL COMPANY of Del.				Connection AIR		Well No. LG-6973	
Pool DIAMOND MOUND ATOKA Mound				Formation ATOKA		Unit B	
Completion Date 11-16-80		Total Depth 8,765		Plug Back TD 8,765		Elevation 3,524 KB	
Csg. Size 4 1/2		ID 11.6		Set At 8,765		Perforations: From 8,340 To 8,484	
Tub. Size 2 3/8		ID 7.4		Set At 8,244		Perforations: From OPEN To	
Type Well - Single - Protionhead - G.G. or G.O. Multiple SINGLE						Packer Set At 8,244	
Producing Thru TUBING		Reservoir Temp. °F 146° 8,418'		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2	
L 8,244		H 8,244		Gg .670		% CO ₂ .341	
				% N ₂ .513		% H ₂ S -0-	
				Prove PLATE 1,875		Meter Run 4"	
						Taps FLANGE	
FLOW DATA				TUBING DATA		CASING DATA	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.
1.	4 X	1.875		500	5	68	2035
2.	4 X	1.875		500	17	69	1624
3.	4 X	1.875		500	35	70	982
4.	4 X	1.875		500	32	68	660
5.							
RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mhd
1.	17.26	50.66	513.2	.9924	1.222	1.054	1,117.6
2.	17.26	93.40	513.2	.9915	1.222	1.054	2,058.7
3.	17.26	134.02	513.2	.9905	1.222	1.054	2,951.1
4.	17.26	128.15	513.2	.9924	1.222	1.054	2,827.2
5.							
NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl. A.P.I. Gravity of Liquid Hydrocarbons _____ Deg. Specific Gravity Separator Gas .670 XXXXXXXXXX Specific Gravity Flowing Fluid XXXXXX Critical Pressure 670 P.S.I.A. _____ P.S.I.A. Critical Temperature 381 R _____ R		
1.	.77	528	1.39	.90			
2.	.77	529	1.39	.90			
3.	.77	530	1.39	.90			
4.	.77	528	1.39	.90			
5.							
$P_c = 3141.2$ $P_c^2 = 9,867.1$					(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.3048$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.2951$		
NO.	P _c ²	P _w	P _w ²	P _c ² - P _w ²	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3,822.0$		
1.	4,195	2,635.2	6,944	2,923			
2.	2,680	2,168.2	4,701	5,166			
3.	990	1,518.2	2,305	7,562			
4.	453	1,153.2	1,330	8,537			
5.							
Absolute Open Flow 3,822.0				Mhd @ 15.025		Angle of Slope 47%	
						Slope, n .972	
Remarks:							
Approved By Commission:		Conducted By: Bo Faulkenberry		Calculated By: Don Bennett		Checked By:	