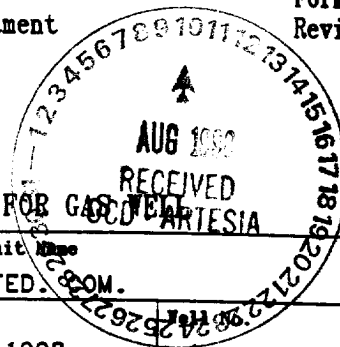


Submit in duplicate to
appropriate district office
see Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-1991

OIL CONSERVATION DIVISION
P.O. Box 2088
Santa Fe, New Mexico 87504-2088



MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS TURKEY TRACK

Operator OXY USA INC				Lease or Unit Name ROSCO FED. COM.			
Test Type ☒ Initial ☐ Annual ☐ Special				Test Date 20-JUL-1998			
Completion Date		Total Depth		Plug Back TD		Elevation	
Csg. Size	Wt.	d	Set At	Perforation: From 8934 To 8958		Unit Ltr - Sec - TWP - Rge. N - 4 - 17S - 27E	
Tbg. Size	Wt.	d	Set At	Perforation: From To		County EDDY	
Type Well-Single-Bradenhead-G.G. or G.O. Multiple				Packer Set At 8779		Pool CROW PLATS TURKEY TRACK (11/1/98)	
Producing Thru TUBING		Reservoir Temp. F 158		Mean Annual Temp. F 60		Baro. Pressure 14.40	
L 8946	H 8946	Gg .626	% CO ₂ .48	% N ₂ .36	% H ₂ S	Prover	Meter Run 3
						Taps FLANGE	

FLOW DATA					TUBING DATA		CASING DATA		SIP/FLOW DURATION (HRS.)
NO.	(PROVER) LINE SIZE x ORIFICE SIZE	PRESS. PSIG	DIFF. h _v	TEMP. F	PRESS. PSIG	TEMP. F	PRESS. PSIG	TEMP. F	
SHUT-IN PRESSURE									
1.	3.00 x 1.50	732.00	.10	84	2660	158	2120		96
2.	3.00 x 1.50	734.50	2.00	84	2461	158	1956	97	1
3.	3.00 x 1.50	744.80	11.20	84	2434	157	1918	100	1
4.	3.00 x 1.50	765.00	27.20	84	2250	152	1737	90	1
					2035	142	1556	92	1

RATE OF FLOW CALCULATIONS								RATE OF FLOW (Q) MCFD
NO.	CORFFICIENT (24 HOUR)	h _w P _m	PRESSURE P _m	FLOW TEMP. FACTOR F _t	GRAVITY FACTOR F _g	SUPER COMPRESS. FACTOR F _{py}		
1.	11.410	8.639	746.4	.9777	1.2639	1.0582		126.9
2.	11.410	38.701	748.9	.9777	1.2639	1.0584		577.5
3.	11.410	92.212	759.2	.9777	1.2639	1.0592		1377.1
4.	11.410	145.601	779.1	.9777	1.2639	1.0608		2177.8

NO.	P _r	TEMP.	T _r	Z
1.	1.110	544	1.495	.8930
2.	1.114	544	1.499	.8927
3.	1.129	544	1.499	.8913
4.	1.159	544	1.499	.8886

Gas-Liquid Hydrocarbon Ratio	70.7	Wcf/bbl
API Gravity of Liquid Hydrocarbons	58.000	Deg.
Specific Gravity Separator Gas	.626	
Specific Gravity Flowing Fluid	.667	
Critical Pressure	672 PSIA	670 PSIA
Critical Temperature	362 R	376 R

P _C =	2134.4	P _C ² =	4555.7
NO.	P _w	P _w ²	P _C ² - P _w ²
1.	1970.7	3883	672.004
2.	1933.2	3737	818.400
3.	1751.9	3069	1486.509
4.	1570.7	2467	2088.564

$$(1) \frac{P_C^2}{P_C^2 - P_W^2} = \frac{2.181}{2.181 - 2.181} = \frac{2.181}{0} = \text{undefined}$$

$$(2) \left[\frac{P_C^2}{P_C^2 - P_W^2} \right]^n = \frac{2.181}{2.181 - 2.181} = \text{undefined}$$

$$AOF = Q \left[\frac{P_C^2}{P_C^2 - P_W^2} \right]^n = \frac{4751}{2.181 - 2.181} = \text{undefined}$$

Absolute Open Flow		4751		Mcf/d @ 15.025	Angle of Slope - 45	Slope, n	1
Remarks Used bottom hole data. Originally calculated "n" was greater than 1; so, default value of 1 was used.							
Approved By Division:		Conducted By: C. TAYLOR		Calculated By: BPT System/SCHLUMBERGER		Checked By: D. SYKES-BOOKHAMMER	