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appropriate district office
See Rule 401 & Rule 1122

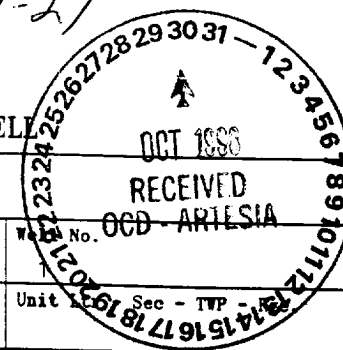
State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-1991

OIL CONSERVATION DIVISION
P.O. Box 2088
Santa Fe, New Mexico 87504-2088

30-015-30240C/SF
F 9-17-27

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL



Operator OXY USA INC					Lease or Unit Name WALLACE STATE				
Test Type ☒ Initial ☐ Annual ☐ Special					Test Date 18-OCT-1998				
Completion Date			Total Depth		Plug Back TD			Elevation	
Csg. Size	Wt.	d	Set At	Perforation: From 8890 To 8992					County EDDY
Tbg. Size	Wt.	d	Set At	Perforation: From To					Pool ARTESIA
Type Well-Single-Bradenhead-G.G. or G.O. Multiple SINGLE					Packer Set At Formation <i>Crow Flats</i> <i>Morrow</i>				
Producing Thru		Reservoir Temp.F 154		Mean Annual Temp.F		Baro. Pressure 14.40		Connection	
L	H	Gg	% CO ₂	% N ₂	% H ₂ S	Prover		Meter Run 3.068	
8941	8941	.648	.49	.36				Taps FLANGE	

FLOW DATA					TUBING DATA		CASING DATA		SIP/FLOW DURATION (HRS.)	
NO.	(PROVER) LINE SIZE x ORIFICE SIZE		PRESS. PSIG	DIFF. h _w	TEMP. F	PRESS. PSIG	TEMP. F	PRESS. PSIG		TEMP. F
SHUT-IN PRESSURE										
1.	3.07	x 1.37	750.30	4.93	73	3401	154			39
2.	3.07	x 1.37	759.00	20.83	73	3176	154	2534	70	1
3.	3.07	x 1.37	763.30	32.97	71	2795	152	2286	70	1
4.	3.07	x 1.37	772.00	75.75	72	2495	147	2003	70	1
						1940	136	1442	70	1

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	h _w P _m	PRESSURE P _m	FLOW TEMP. FACTOR F _t	GRAVITY FACTOR F _g	SUPER COMPRESS. FACTOR F _{py}	RATE OF FLOW (Q) MCFD
1.	9.486	61.400	764.7	.9877	1.2423	1.0701	764.8
2.	9.486	126.925	773.4	.9877	1.2423	1.0710	1582.2
3.	9.486	160.127	777.7	.9896	1.2423	1.0725	2002.7
4.	9.486	244.069	786.4	.9887	1.2423	1.0728	3050.5

NO.	P _r	TEMP.	T _r	Z
1.	1.139	533	1.441	.8733
2.	1.152	533	1.441	.8719
3.	1.158	531	1.435	.8694
4.	1.171	532	1.438	.8689

Gas-Liquid Hydrocarbon Ratio	30.6	Mcf/bbl
API Gravity of Liquid Hydrocarbons	40.000	Deg.
Specific Gravity Separator Gas	.648	
Specific Gravity Flowing Fluid	.757	
Critical Pressure	671 PSIA	666 PSIA
Critical Temperature	369 R	404 R

P _C =	3415.7	P _C ² =	11667.0
NO.	P _w	P _w ²	P _C ² - P _w ²
1.	3190.4	10178	1488.355
2.	2809.4	7892	3774.279
3.	2509.4	6297	5369.918
4.	1954.4	3819	7847.327

$$(1) \frac{P_C^2}{P_C^2 - P_W^2} = \frac{1.487}{1.383}$$

$$(2) \left[\frac{P_C^2}{P_C^2 - P_W^2} \right]^n = 1.383$$

$$AOF = Q \left[\frac{P_C^2}{P_C^2 - P_W^2} \right]^n = 4218$$

Absolute Open Flow		4218		Mcf/d @ 15.025		Angle of Slope - 50.7		Slope, n .817	
Remarks									
Approved By Division:			Conducted By: <i>Charles Taylor</i>			Calculated By: BPT System/SCHLUMBERGER			Checked By: <i>Paul Taylor-Rodhamer</i>