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appropriate district office
See Rule 401 & Rule 1122

Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

31-015-30532

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator MURCHISON OIL & GAS					Lease or Unit Name MARALO FED				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 2/13/99		Well No. 2		
Completion Date		Total Depth		Plug Back TD 9544		Elevation		Unit Ltr. - Sec. - Twp. - Rge. 22 - 17S - 27-E	
Csg. Size 5 1/2		Wt. 17#		Set At		Perforations: From: 9372 To: 9402		County EDDY	
Tbg. Size 2 7/8		Wt. 6.5		Set At 2.441		Perforations: From: To:		Pool Logan Draw MOR	
Type Well - Single - Bradenhead - G.G. or G.C. Multiple single					Packer Set At 9235		Formation MORROW		
Producing Thru TBG		Reservoir Temp. °F 147.9		Mean Annual Temp. °F 60°		Baro. Press. - P 13.2		Connection AIR	
L 9235	II 9235	Gg .766	% CO ₂ 7.717	% N ₂ .342	% H ₂ S -0-	Prover -0-	Water Run 3.068	Taps FWG	
FLOW DATA					TUBING DATA				
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Duration of Flow
1.	3.068 X 1.750	595.3	1"	76°	2615	"	76°	2540	60 min
2.	3.068 X 1.750	633.7	2.25"	76°	2540	"	90°	2430	60 min
3.	3.068 X 1.750	673.3	4"	90°	2430	"	88°	2010	60 min
4.	3.068 X 1.750	558.1	16.8"	88°	2010	"			60 min
5.									
RATE OF FLOW CALCULATIONS									
NO.	COEFFICIENT (24 HOUR)	$\frac{h_w}{P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd		
1.	15.61	24.39	595.3	.9850	1.143	1.063	455		
2.	15.61	37.76	633.7	.9850	1.143	1.063	705		
3.	15.61	51.89	673.3	.9723	1.143	1.060	954		
4.	15.61	96.83	558.1	.9741	1.143	1.059	1782		
5.									
NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio 81.167 Mcf/bbl				
1.	.77	536	1.34	.885	A.P. I. Gravity of Liquid Hydrocarbons 56.8 Deg				
2.	.77	536	1.34	.885	Specific Gravity Separator Gas .7660 XXXXXXXXXX				
3.	.79	550	1.37	.890	Specific Gravity Flowing Fluid N/A XXXXXX				
4.	.78	548	1.37	.892	Critical Pressure 696 P.S.I.A. P.S.I.A.				
5.					Critical Temperature 400 R R				
P _c 2692.6 P _c ² 7250.0									
NO.	P _r ²	P _w	P _w ²	P _c ² - P _w ²	1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.24$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.90$				
1.		2571.0	6610.0	640.0	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3385.8$				
2.		2529.2	6396.8	853.2					
3.		2437.8	5942.8	1307.2					
4.		2004.0	4016.0	3234.0					
5.									
Absolute Open Flow 3385.8 Mcfd @ 15.025					Angle of Slope θ 51.29			Slope, n .801	
Remarks: * CALCULATED FROM KNOWN BOTTOM HOLE PRESSURES									
* WELL MADE 2 BBLS OF 56.8 API GRAVITY CONDENSATE									
Approved By Division			Conducted By: PRO WELL TESTING			Calculated By: MB		Checked By: BM	