

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

c/514

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 7/22/00		RECEIVED OCD - ARTESIA 30-015-30722	
Company OXY USA, INC.				Connection 6-10-00					
Pool Hobbs Logan Draw Morrow				Formation MORROW				Unit	
Completion Date 6/10/00		Total Depth 9480'		Plug Back TD 9417'		Elevation 3461		Farm or Lease Name HAM OXY IJAM State	
Csg. Size 4 1/2"	Wt. 11.6#	d	Set At 9450'	Perforations: From 9129 To 9152		Well No. 1			
Tbg. Size 2.375	Wt. 4.7	d 1.995	Set At 9079	Perforations: From To		Unit Sec. Twp. Rge. I 16 17S 27E			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE						Packer Set At 9068		County EDDY	
Producing Thru TUBING		Reservoir Temp. °F 154 @ 9095		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State NM	
L 9095	H 9095	G _g 0.65	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run 4.026	Taps FLANGE	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2492	69			94
1	4.026	3.0		352	0.4	94	2438	81			1
2	4.026	3.0		352	0.8	94	2401	88			1
3	4.026	3.0		360	2.7	79	2288	88			1
4	4.026	3.0		371	6.3	68	2087	91			1
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RATE OF FLOW CALCULATIONS							
NO	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super. Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	51.64	12.08	364.9	0.9687	1.2403	1.0304	772
2	51.64	17.09	364.9	0.9686	1.2403	1.0304	1092
3	51.64	31.74	373.1	0.9820	1.2403	1.0346	2065
4	51.64	49.19	384.1	0.9923	1.2403	1.0379	3245
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NO	P _r	Temp °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1	0.54	554	1.48	0.943	118.828	
2	0.54	554	1.48	0.943	62.6	
3	0.56	539	1.44	0.936		
4	0.57	528	1.41	0.929		
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A.P.I. Gravity of Liquid Hydrocarbons 62.6 Deg. Specific Gravity Separator Gas 0.650 Specific Gravity Flowing Fluid XXXX Critical Pressure 670 P.S.I.A. 669 P.S.I.A. Critical Temperature 374 R 381 R			
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$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 3.7094$ $(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.8320$ $AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 9190$
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NO	P _r ²	P _w ²	P _w ²	P _c ² - P _w ²
1	2483	6163	284	
2	2453	6020	428	
3	2346	5505	942	
4	2170	4710	1738	
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Absolute Open Flow 9190 Mcfd @ 15.025	Angle of Slope θ 51.5	Slope, n 0.7941
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Remarks Bottomhole pressures recorded using electronic pressure gauge #P-50.			
Approved By Commission	Conducted By: ARC Pressure Data, Inc.	Calculated By: Rod Dodson	Checked By: