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appropriate district office.
See Rule 401 & Rule 1122

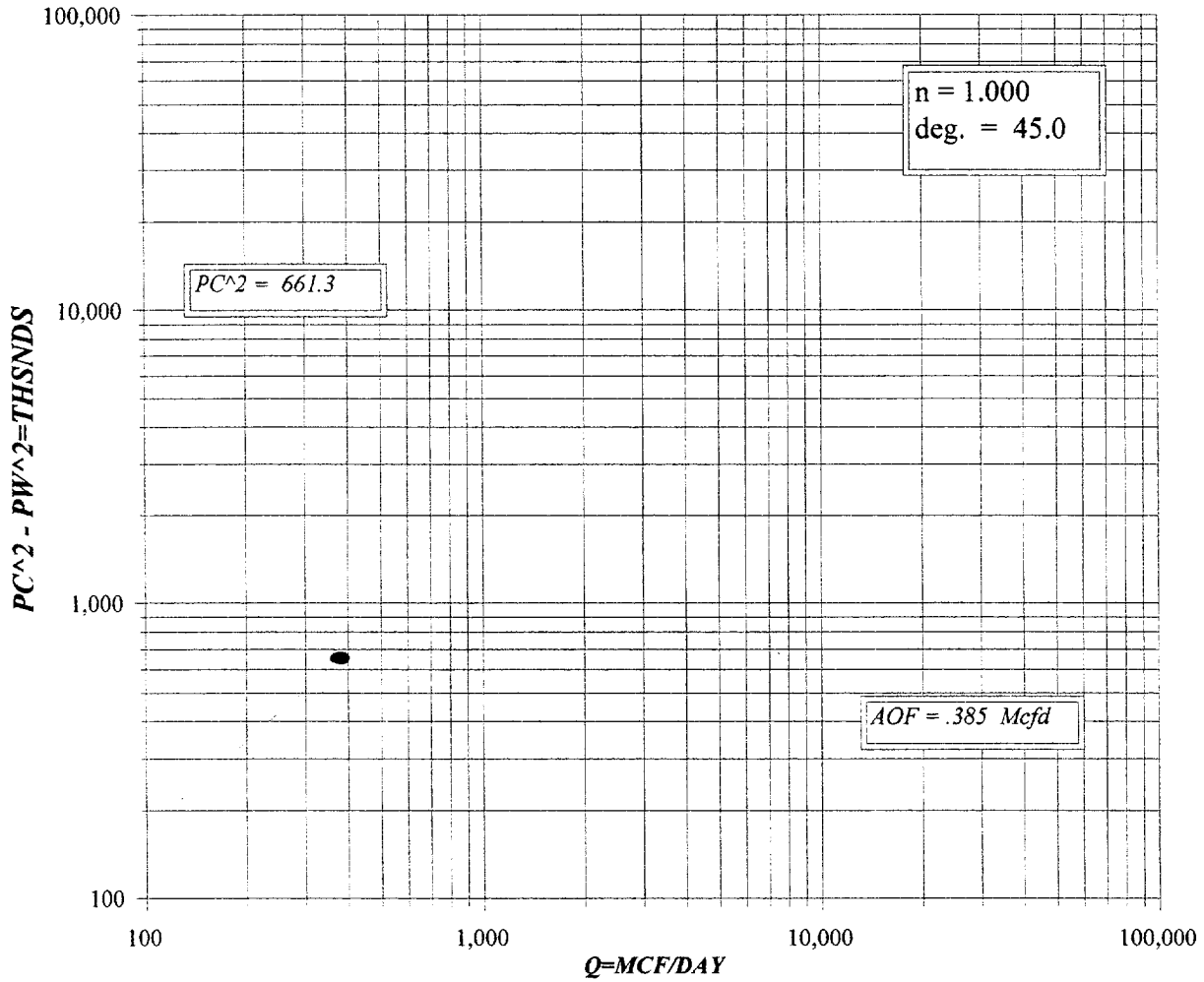
State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

Form C-122
Revised October, 1999

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator MEWBOURNE OIL /				Lease or Unit Name EMPIRE "18" FED COM			
Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 2/20/01		Well No. 2	
Completion Date 2/18/01		Total Depth 10800		Plug Back TD 10711		Elevation 3675	
Unit Ltr - Sec - TWP - Rge LOT 3 18-17S-29E		County EDDY					
Csg. Size 5 1/2	Wt. 17	d 4.892	Set At 10800	Perforations: From: 10599 To: 10606		Pool SOUTH EMPIRE	
Tbg. Size 2 7/8	Wt. 6.5	d 2.441	Set At 10366	Perforations: From: To:		Formation MORROW	
Type Well-Single-Bradenhead-G.G. or G.O. Multiple SINGLE				Packer Set At 10325		Connection SALES	
Producing Thru TUBBING		Reservoir Temp. °F 177.4		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2	
L 10366	H 10366	Gg 0.722	%CO ₂ 5.814	%N ₂ 2.302	%H ₂ S N/A	Prover N/A	Meter Run 3.067
Taps FLG							
FLOW DATA				TUBING DATA		CASING DATA	
No.	Prover Line Size	Orifice x Size	Press p.s.i.g.	Diff. h _w	Temp. °F	Press p.s.i.g.	Temp. °F
SI						800	N/A
1	3.067 X 1.125		80	17	66	70	PKR
2							N/A
3							
4							
5							
RATE OF FLOW CALCULATIONS							
No.	COEFFICIENT (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress Factor F _{pv}	Rate of Flow Q, Mcfd
1							380
2							
3	TOTAL	FLOW	METER				
4							
5							
No.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio N/A Mcf/bbl.		
1					A.P. I. Gravity of Liquid Hydrocarbons Deg.		
2	TOTAL	FLOW	METER		Specific Gravity Separator Gas 0.722 XXXXXXXX		
3					Specific Gravity Flowing Fluid XXXXXX		
4					Critical Pressure 688 P.S.I.A. P.S.I.A.		
5					Critical Temperature 385 R. R.		
P _c 813.2 P _{c2} 661.3							
No.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $P_c^2 = \frac{1.014}{P_c^2 - P_w^2}$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.014$		
1	69	94.9	9	652.3			
2							
3							
4							
5							
Absolute Open Flow 0.385				Mcf/d @ 15.025		Angle of Slope (°): 45	
				Slope n:		1	
Remarks: * NO LIQUID MADE DURING TEST.							
Approved By Division:		Conducted By: PRO WELL TESTING		Calculated By: MERV BUECKER		Checked By: BM	

MEWBOURNE OIL
EMPIRE "18" FED COM # 2



COMPANY :MEWBOURNE OIL LEASE :EMPIRE "18"FED WELL NO. : 2
UNIT :LOT 3 SECTION : 18 TOWNSHIP :17S
L : 10336 H : 10336 L/H : 1 G/GMIX : 0.722
%CO2 : 5.814 %N2 : 2.302 H2S : DATE :12/20/01
d : 2.441 Fr :0.010763 GH : 7462.6 RANGE :29E

VOL 1 : 380 PSIA 1 : 83.2 RESV.TEMP 177.4
VOL 2 : PSIA 2 :
VOL 3 : PSIA 3 : SHUT-IN PR= 813.2
VOL 4 : PSIA 4 :

PCR : 688
TCR : 385

Pc = 813.2 Pc2 = 661.3 *
Pt2 = 6.9 Pw = 94.9 *
0.0 ERR *
0.0 ERR *
0.0 ERR *

Pc2-Pw2= 652.3 Pw2 = 9.0 *
ERR ERR *
ERR ERR *
ERR ERR *

n = 1.000

Pc2/(Pc2-Pw2) = 1.014
ERR
ERR
ERR

[Pc2/Pc2-Pw2]n = 1.014
ERR
ERR
ERR

AOF= Q 0.385
ERR
ERR
ERR

FORM C122-D

LINE	RATE 1		RATE 2		RATE 3		RATE 4	
	1ST	2ND	1ST	2ND	1ST	2ND	1ST	2ND
1 QM	0.380	0.380	0.000	0.000	0.000	0.000	0.000	0.000
2 TW	534	534	534	534	534	534	534	534
3 Ts	637.4	637.4	637.4	637.4	637.4	637.4	637.4	637.4
4 T	585.7	585.7	585.7	585.7	585.7	585.7	585.7	585.7
PR (est)	0.12	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5 Z(est)	0.964	0.962	ERR	ERR	ERR	ERR	ERR	ERR
6 TZ	564.8	563.2	ERR	ERR	ERR	ERR	ERR	ERR
7 GH/TZ	13.214	13.249	ERR	ERR	ERR	ERR	ERR	ERR
8 eS	1.641	1.644	ERR	ERR	ERR	ERR	ERR	ERR
9 l-e-S	0.391	0.392	ERR	ERR	ERR	ERR	ERR	ERR
10 Pt	83.2	83.2	0.0	0.0	0.0	0.0	0.0	0.0
11 Pt2 /1000	6.9	6.9	0.0	0.0	0.0	0.0	0.0	0.0
12 Fr	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.0107631
13 Fc=FrTZ	6.079	6.062	ERR	ERR	ERR	ERR	ERR	ERR
14 FcQm	2.31	2.30	ERR	ERR	ERR	ERR	ERR	ERR
15 L/H(FcQm)	5.3	5.3	ERR	ERR	ERR	ERR	ERR	ERR
16 Fw	2.084763	2.077905	ERR	ERR	ERR	ERR	ERR	ERR
17 Pw2	9.0	9.0	ERR	ERR	ERR	ERR	ERR	ERR
18 Ps2	14.8	14.8	ERR	ERR	ERR	ERR	ERR	ERR
19 Ps	121.6	121.6	ERR	ERR	ERR	ERR	ERR	ERR
20 P	102.4	102.4	ERR	ERR	ERR	ERR	ERR	ERR
21 Pr	0.15	0.15	ERR	ERR	ERR	ERR	ERR	ERR
22 Tr	1.52	1.52	1.52	1.52	1.52	1.52	1.52	1.52
23 Z	0.962	0.962	ERR	ERR	ERR	ERR	ERR	ERR