

MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

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Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 10-20-71		DEC 2 1971	
Company David Fasken				Connection None			
Pool West Atoka (Morrow)				Formation Morrow			
Completion Date 9-22-71		Total Depth 8920		Plug Back TD 8854		Elevation 3445 Gr	
Csg. Size 4 1/2		Wt. 11.60		Set At 8919		Perforations: From 8708 To 8757	
Tub. Size 2 7/8		Wt. 6.50		Set At 7495		Perforations: From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 7495		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 152 @ 8600		Mean Annual Temp. °F 70		Baro. Press. - P _a 13.2	
L 8733		H 8733		Gg 0.613		% CO ₂ % N ₂ % H ₂ S	
						Prover 2"	
						Meter Run Taps	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI				2309			2309				
1.	2"	X	1/16"	2239		67	2239	67			60 Min.
2.	2"	X	3/32"	2162		70	2162	70			60 Min.
3.	2"	X	1/8 "	1997		72	1997	72			90 Min.
4.	2"	X	3/16"	1605		71	1605	71			60 Min.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	0.06405		2252.2	0.9933	1.277	1.156	211.5
2.	0.1410		2175.2	0.9905	1.277	1.151	446.5
3.	0.2648		2010.2	0.9887	1.277	1.147	770.9
4.	0.6082		1618.2	0.9896	1.277	1.131	1406.7
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Dry Gas	Mcf/bbl.
1.	3.36	527	1.46	0.746	A.P.I. Gravity of Liquid Hydrocarbons	None	Deg.
2.	3.24	530	1.46	0.747	Specific Gravity Separator Gas	0.613	XXXXXXXXXX
3.	3.00	532	1.47	0.758	Specific Gravity Flowing Fluid	XXXXXX	
4.	2.41	531	1.47	0.782	Critical Pressure	671 P.S.I.A.	P.S.I.A.
5.					Critical Temperature	362 R	R

NO.	P _t ²	P _s ²	P _s ²	P _f ² - P _s ²
1		2901.2	8417	393
2		2810.2	7897	913
3		2645.2	6997	1813
4		2313.2	5351	3459
5				

(1) $\frac{P_c^2}{P_c^2 - R_w^2} = \frac{P_c^2}{P_c^2 - R_w^2}$ (2) $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n =$

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U. S. GEOLOGICAL SURVEY
ARTESIA NEW MEXICO

Absolute Open Flow <u>3150</u> Mcfd @ 15.025		Angle of Slope @ <u>49° 12'</u>		Slope, n <u>0.8633</u>	
Remarks:					
Approved By Commission:		Conducted By: Tefteller, Inc		Calculated By: Farrest Tefteller	
Checked By:					