

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 11-7-72		NOV 28 1972	
Company Falcon Oil Corporation				Location None yet		O. G. C. SARTESIA, OFFICE	
Pool Atoka (Penn)				Structure Strawn			
Completion Date 11-4-72		Total Depth 9191'		Packer Set At 9148' KB		Elevation 3319' GL	
Casing Size 4 1/2"		Wt. 11.6# 10.5#		Set At 4.000 4.052		Perforations: From 8968' To 8978'	
Tubg. Size 2 3/8"		Wt. 4.7#		Set At 1.995 8944'		Perforations: From open end To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple G.G. Multiple				Packer Set At 8931' KB 8935' KB		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 60		Mech. Annul. Temp. °F 13.2		Baro. Press. - P _a New Mexico	
L 8944	H 8944	G _g .782	% CO ₂ .49	% N ₂ .26	% H ₂ S 0	Prover X	Meter Run Flange

FLOW DATA						TUBING DATA		CASING DATA		Duration	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. in. H ₂ O	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	of Flow
1.	3"		2.25	300	22.5	78	1615	72	0		30 min
2.	3"		2.25	310	28.	80	1545	72	0		45 min
3.	3"		2.25	320	36.	79	1414	72	0		60 min
4.	3"		2.25	320	37.	78	1298	72	0		30 min
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1.	28.78	106.06	313.2	.9831	1.131	1.071	3,635
2.	28.78	119.50	323.2	.9813	1.131	1.073	4,096
3.	28.78	136.82	333.2	.9822	1.131	1.075	4,698
4.	28.78	138.07	333.2	.9831	1.131	1.075	4,750
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio 368 Mcf/bbl.
1.	.77	538	1.29	.871	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.	.79	540	1.29	.868	Specific Gravity Separator Gas .782 XXXXXXXXXX
3.	.80	539	1.29	.866	Specific Gravity Flowing Fluid XXXXX
4.	.80	538	1.29	.866	Critical Pressure 666 P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature 418 °R _____ °R

NO.	P _t ²	P _w ²	P _w ²	P _t ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 4.264$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.412$
1.	2274.2	5172	969		ACTUAL $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 11,332$	
2.	2233.2	4987	1154			
3.	2168.2	4701	1440			
4.	2117.2	4483	1658			
5.						

Absolute Open Flow 11,332 Mcfd @ 15.025	Angle of Slope θ 58.5	Slope, n .613
Remarks: P_t Substituted for P_w Measured with Amerada RPG-3 Instrument @ 8973'		
Approved By Commission:	Conducted By: Massey	Calculated By: Massey
		Checked By: