

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form 2-122
Revised 9-1-65
C-122

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 2-19-76		MAR 1 1976	
Company Amoco Production Company				Connection Natural Gas Pipeline of America			
Pool Red Lake				Formation Penn.		Unit ARTESIA, OFFICE	
Completion Date 1-2-75		Total Depth 9418'		Plug Back TD 9362'		Elevation 3405 K.B.	
Farm or Lease Name Hondo "B" Fed. Gas Com.							
Csg. Size 5 1/2"	Wt. 17#	Set At 9408'	Perforations: From 9314' To 9343'		Well No. 1		
Tbg. Size 2 3/8"	Wt. 4.6#	Set At 9263'	Perforations: From open To ended		Unit L	Sec. 8	Twp. 18S
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single					Packer Set At 9255'		County Eddy
Producing Thru Tubing		Reservoir Temp. °F 208° @ 9329'		Mean Annual Temp. °F 60°		Baro. Press. - P _g 13.2	
State New Mexico							
L 9329'	H 9329'	G _g 0.5899	% CO ₂ 0.428	% N ₂ 0.803	% H ₂ S --0--	Prover ----	Meter Run 4" X 2.00"
						Taps Flange	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							2770.0		Packer	Choke	
1.	4" X 2.00"			600.0	8.0	65	2631.0	68		12/64"	45 Min.
2.	4" X 2.00"			600.0	16.0	65	2522.0	70		14/64"	45 Min.
3.	4" X 2.00"			600.0	29.0	65	2329.0	72		17/64"	45 Min.
4.	4" X 2.00"			620.0	54.0	65	1947.0	72		22/64"	45 Min.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super. Compress. Factor, F _{pv}	Rate of Flow Q, Mscf
1	19.81	70.04	613.2	.9952	1.302	1.051	1890
2	19.81	99.05	613.2	.9952	1.302	1.051	2672
3	19.81	133.35	613.2	.9952	1.302	1.051	3598
4	19.81	184.91	633.2	.9952	1.302	1.052	4993
5.							

NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	0.91	525	1.48	.905	53.75	60.1	0.5899	X X X X X X X X	672	354
2.	0.91	525	1.48	.905				X X X X X		
3.	0.91	525	1.48	.905						
4.	0.94	525	1.48	.903						
5.										

P _f 3476.2 P _s 12084				(1) $\frac{P_f^2}{P_f^2 - P_s^2} = 2.826$		(2) $\left[\frac{P_f^2}{P_f^2 - P_s^2} \right]^n = 1.885$	
NO.	P _f ²	P _s ²	P _s ²	P _f ² - P _s ²			
1	6992	3336.2	11130	954			
2	6427	3244.2	10525	1559			
3	5486	3082.2	9500	2584			
4	3842	2794.2	7808	4276			
5							

AOF = Q $\left[\frac{P_f^2}{P_f^2 - P_s^2} \right]^n = 9412$				Absolute Open Flow 9412 Mscf @ 15.025		Angle of Slope θ 58.6°	
				Slope, n 0.610			

Remarks: Bottom hole pressure measured with amerada gauge @ 9329 feet.

Approved by Commission:	Conducted By: Don Tyson	Calculated By: R. West	Checked By: J.W.W.
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