

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test: ☒ Initial ☐ Annual ☐ Special				Test Date: 7-30-75		RECEIVED AUG 14 1975	
Company: Mark Production Company				Connection: No			
Pool: West Red Lake				Formation: Atoka Morrow		Unit: O.C.C.	
Completion Date: 7-22-75		Total Depth: 9150		Plug Back TD: 9110		Elevation: GL 3289	
Csg. Size: 4- 1/2		Wt.: 11.6		Set At: 9150		Perforations: From 8914 To 8931	
Tub. Size: 2-3/8 eve		Wt.: 4.7		Set At: 8824		Perforations: From To	
Type Well - Single - Bradenhead - G.C. or G.O. Multiple: Single				Packer Set At: 8814		County: Eddy	
Producing Thru: Tubing		Reservoir Temp. °F: 162 @ 8920		Mean Annual Temp. °F: 60		Baro. Press. - P _a : 13.2	
L: 8923		H: 8923		G _g : .652		% CO ₂ : % N ₂ : % H ₂ S: Prover: Meter Run: Taps:	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prever Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2751	84°			
1.	3.0		2.25	315	1"	68	2602	78°			1 hour
2.	3.0		2.25	325	4"	61	2387	81°			1 hour
3.	3.0		2.25	325	11"	59	1912	82°			1 hour
4.	3.0		2.25	330	19"	66	1536	82°			1 hour
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcf/d
1	28.78	18.116	328.2	.9924	1.2384	1.032	662
2	28.78	36.780	338.2	.9990	1.2384	1.034	1354
3	28.78	60.993	338.2	1.0010	1.2384	1.041	2265
4	28.78	80.751	343.2	.9943	1.2384	1.034	2959
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	.49	528	1.41	.939	72866	54.2 @ 60°	.652	X X X X X X X X	670	375
2	.50	521	1.39	.935				X X X X X		
3	.50	519	1.38	.923						
4	.51	526	1.40	.936						
5										

NO.	P _r ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$
1	2764.2	2620.7	6868	773	1.54738	1.42030
2		2423.7	5874	1767		
3		1980.8	3924	3717		
4		1644.1	2703	4938		
5						

Absolute Open Flow: 4203 Mcf/d @ 15.025 Angle of Slope: 51° 14' Slope, n: .803

Remarks:

Approved By Commission:	Conducted By: I. N. Casneris	Calculated By: H. L. Haaler	Checked By:
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