

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELLS

45F. File
Form C-112
Revised 8-1-84

RECEIVED BY

AUG 09 1984

O. C. D.

ARTESIA, OFFICE

Type Test ☐ Initial ☒ Annual ☐ Special				Test Date 8-1-84																																					
Company Gulf Oil Exp. & Prod. Co.				Correlation Air																																					
Pool Pinedale Drive - Pinedale - Penn				Formation Penn																																					
Completion Date 7-27-84		Total Depth 8708		Plug back TD 8450 8415																																					
Csg. Size 5 1/2		Set At 8708		Elevation 3643' 6"																																					
Trq. Size 2 3/8		Set At 6522		Perforations: From 6582 To 6982																																					
Type Well - Single - Pradenthead - G.G. or G.O. Multiple Single Gas				Packer Set At 6522																																					
Producing Thru tbq		Reservoir Temp. °F 139 @ 6522		Mean Annual Temp. °F 60																																					
L 6522		H 6522		Buro. Press. - P _g 13.2																																					
G _g .7769		% CO ₂ 2.236		% N ₂ 10.570																																					
Prover 3"		Meter Run 3"		Turns flg																																					
FLOW DATA																																									
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow																														
SI							1182				28 hrs																														
1.	3 x .500			540	26.0	105	1095				1 hr																														
2.	3 x .500			540	33.5	98	1012				1 hr																														
3.	3 x .500			540	45.5	91	915				1 hr																														
4.	3 x .500			540	59.0	84	800				1 hr																														
5.																																									
RATE OF FLOW CALCULATIONS																																									
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mgd																																		
1	1.183	119.93	553.2	.9594	1.134	1.048	162																																		
2	1.183	136.13	553.2	.9653	1.134	1.050	185																																		
3	1.183	158.65	553.2	.9715	1.134	1.053	218																																		
4	1.183	180.66	553.2	.9777	1.134	1.056	250																																		
5																																									
<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th>NO.</th> <th>P_t</th> <th>Temp. °R</th> <th>T_r</th> <th>Z</th> <th>Gas Liquid Hydrocarbon Ratio</th> <th>Mcf/bbl.</th> </tr> <tr> <td>1.</td> <td>.84</td> <td>565</td> <td>1.47</td> <td>.911</td> <td rowspan="5">dry</td> <td rowspan="5"></td> </tr> <tr> <td>2.</td> <td>.84</td> <td>558</td> <td>1.45</td> <td>.907</td> </tr> <tr> <td>3.</td> <td>.84</td> <td>551</td> <td>1.43</td> <td>.902</td> </tr> <tr> <td>4.</td> <td>.84</td> <td>544</td> <td>1.41</td> <td>.897</td> </tr> <tr> <td>5.</td> <td></td> <td></td> <td></td> <td></td> </tr> </table>								NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.	1.	.84	565	1.47	.911	dry		2.	.84	558	1.45	.907	3.	.84	551	1.43	.902	4.	.84	544	1.41	.897	5.				
NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.																																			
1.	.84	565	1.47	.911	dry																																				
2.	.84	558	1.45	.907																																					
3.	.84	551	1.43	.902																																					
4.	.84	544	1.41	.897																																					
5.																																									
<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th>NO.</th> <th>P_t</th> <th>P_w</th> <th>P_w²</th> <th>P_t² - P_w²</th> <th>(1) $\frac{P_t^2}{P_t^2 - P_w^2} =$</th> <th>(2) $\left[\frac{P_t^2}{P_t^2 - P_w^2} \right]^n =$</th> </tr> <tr> <td>1</td> <td></td> <td>1108.4</td> <td>1228.7</td> <td>199.8</td> <td rowspan="5">3.793</td> <td rowspan="5">1.948</td> </tr> <tr> <td>2</td> <td></td> <td>1025.6</td> <td>1051.9</td> <td>376.6</td> </tr> <tr> <td>3</td> <td></td> <td>928.8</td> <td>862.7</td> <td>565.8</td> </tr> <tr> <td>4</td> <td></td> <td>814.2</td> <td>662.9</td> <td>765.6</td> </tr> <tr> <td>5</td> <td></td> <td></td> <td></td> <td></td> </tr> </table>								NO.	P _t	P _w	P _w ²	P _t ² - P _w ²	(1) $\frac{P_t^2}{P_t^2 - P_w^2} =$	(2) $\left[\frac{P_t^2}{P_t^2 - P_w^2} \right]^n =$	1		1108.4	1228.7	199.8	3.793	1.948	2		1025.6	1051.9	376.6	3		928.8	862.7	565.8	4		814.2	662.9	765.6	5				
NO.	P _t	P _w	P _w ²	P _t ² - P _w ²	(1) $\frac{P_t^2}{P_t^2 - P_w^2} =$	(2) $\left[\frac{P_t^2}{P_t^2 - P_w^2} \right]^n =$																																			
1		1108.4	1228.7	199.8	3.793	1.948																																			
2		1025.6	1051.9	376.6																																					
3		928.8	862.7	565.8																																					
4		814.2	662.9	765.6																																					
5																																									
Absolute Open Flow <u>360</u> Mgd @ 15.025 Angle of Slope <u>63.5</u> Slope, n <u>.500</u>																																									
Remarks:																																									
<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th>Approved By Commission:</th> <th>Conducted By:</th> <th>Calculated By:</th> <th>Checked By:</th> </tr> <tr> <td></td> <td>B & D Well Testers</td> <td>Rick Pagan</td> <td></td> </tr> </table>								Approved By Commission:	Conducted By:	Calculated By:	Checked By:		B & D Well Testers	Rick Pagan																											
Approved By Commission:	Conducted By:	Calculated By:	Checked By:																																						
	B & D Well Testers	Rick Pagan																																							

Post ED-2
8-24-84
Camp, Penn