

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 8/11/78		AUG 18 1978			
Company Gulf Oil Corporation						Connection Air		Unit O.C.C.			
Pool Undesignated						Formation Cisco		ARTESIA, OFFICE			
Completion Date 7-26-78			Total Depth 2680		Plug Back TD 7972		Elevation 3611		Farm or Lease Name Eddy G.X. State Comm.		
Csg. Size 5 1/2		Wt. 15		Set At 8630		Perforations: From 6772 To 6818		Well No. # 1			
Tbg. Size 2 3/8		Wt. 4.7		Set At 6694		Perforations: From To		Unit 0		Sec. Twp. Rge. 18 18 25	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 6694		County Eddy			
Producing Thru Tubing			Reservoir Temp. °F 141 @ 6694		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2		State New Mexico		
L 6694		H 6694		Gg .655		% CO ₂ .28		% N ₂ 2.20		% H ₂ S	
								Prover		Meter Run 4	
										Taps Flange	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	of Flow
SI							1865				72 Hr
1.	4	X	1.250	600	4.0	85	1745				1 Hr
2.	4	X	1.250	630	8.0	83	1615				1 Hr
3.	4	X	1.250	625	16.0	79	1400				1 Hr
4.	4	X	1.250	625	32.0	78	825				1 Hr
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	7.469	49.53	613.2	.9768	1.236	1.057	472
2	7.469	71.73	643.2	.9786	1.236	1.059	636
3	7.469	101.05	638.2	.9822	1.236	1.061	967
4	7.469	142.91	638.2	.9831	1.236	1.061	1376
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcft/bbl.
1	.92	545	1.44	.895	57.887	
2	.96	543	1.44	.891	61.6 @ 60	
3	.95	539	1.43	.889		
4	.95	538	1.42	.888		
5.						

NO.	P _r	P _w	P _w ²	P _r ² - P _w ²	Specific Gravity Separator Gas	XXXXXXX
1		1759.5	3095.8	431.8	Specific Gravity Flowing Fluid	XXXXX
2		1631.2	2660.7	866.9	Critical Pressure	670 P.S.I.A.
3		1420.2	2017.0	1510.6	Critical Temperature	378 °R
4		864.5	747.4	2780.2		
5						

(1) $\frac{P_r^2}{P_r^2 - P_w^2} = 1.269$

AOF = Q $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 1.585$

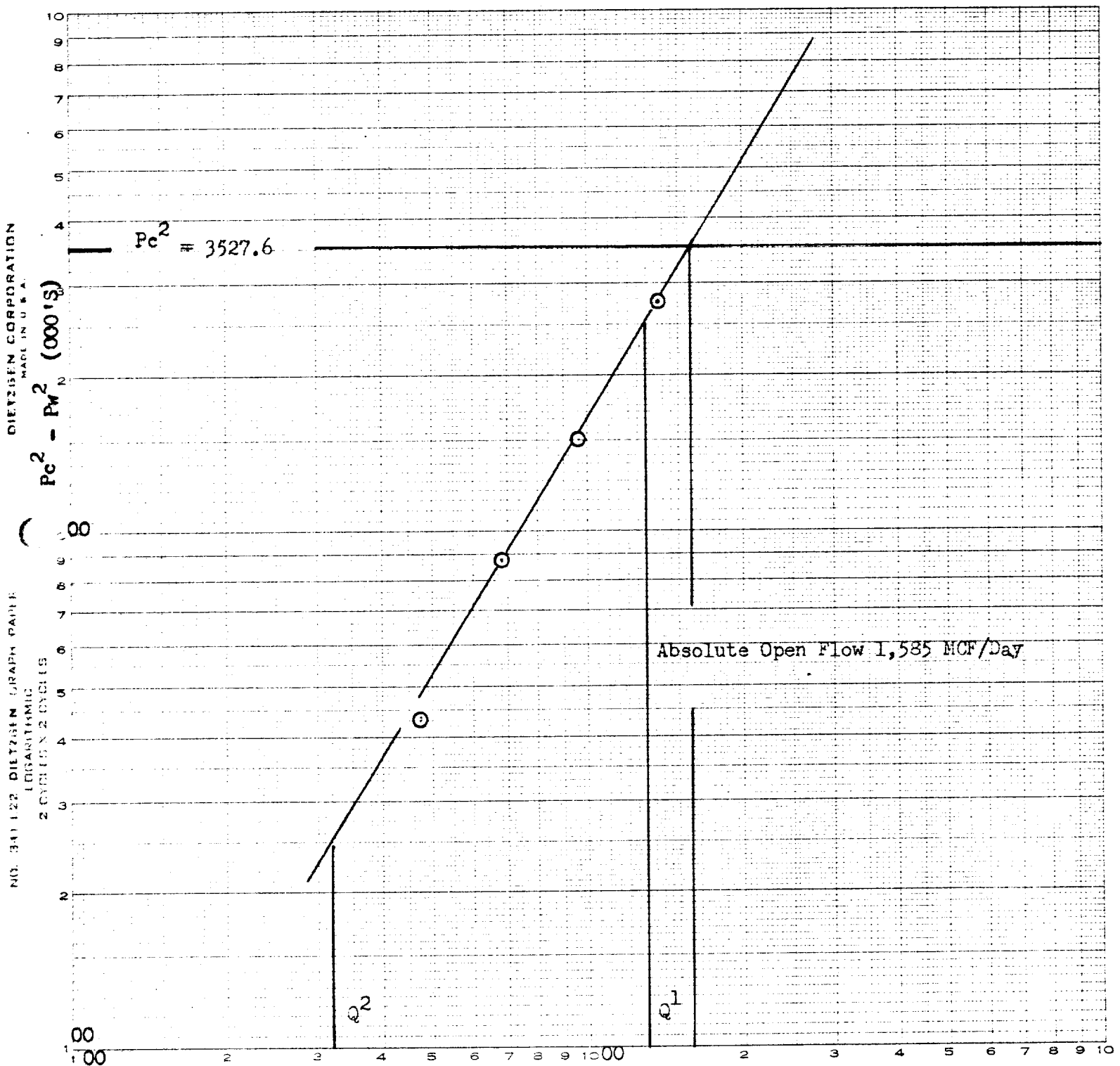
(2) $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 1.152$

Produced 2.52 Ebls of distillate during the test

Absolute Open Flow	1,585	Mcft @ 15.025	Angle of Slope °	59.25°	Slope, n	.595
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Approved By Commission:	Conducted By: Larry Davis	Calculated By: Larry Davis	Checked By:
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Company: Gulf Oil Corporation
 Lease: Eddy GX State Comm
 Well No: # 1
 Field: Undesignated
 County: Eddy
 Date: 8/11/78



$Q = \text{MCF/Day}$
 $Q^1 = 1300$; $\text{Log Of } Q^1 = 3.113943$
 $Q^2 = 330$; $\text{Log Of } Q^2 = \underline{2.518514}$
 $N = .595$

Date Secured 8-11-78	Secured by Day	Department	
Date Run 8-11-78	Run by Bond	Checked by	
Source Press.	Bomb Press.	Source Temp.	Atmos. Temp.

BTU @ 14.696		Actual	Calculated, Dry		SP. GR. @ 14.696 & 60° F		Actual	Calculated	
			1128.92					.655	
Hydrogen Sulphide as grs. H ₂ S/ 100 SCF			Mercaptan as grs. Sulfur/100 SCF			Total		Sweet	
.19 grs			00			.19 grs			
VAPOR PRESS. @ 100° F		Actual, Reid	Calculated						

COMPONENT		MOLE %	GPM	LIQ. VOL. %
Helium	HE ₂			
Hydrogen Sulphide	H ₂ S			
Carbon Dioxide	CO ₂	.28		
Nitrogen	N ₂	2.20		
Methane	C ₁	85.25		
Ethane	C ₂	7.73		
Propane	C ₃	3.01		
Iso Butane	IC ₄	.38		
Normal Butane	C ₄	.76		
Iso Pentane	IC ₅	.18		
Normal Pentane	C ₅	.17		
Hexane	C ₆	.04		
Heptane	C ₇			
		100%		

DISTRIBUTION

ENGLER	
IBP	% @ 96
5	% @ 140
10	% @ 275
20	End Point
30	Recovery
40	Residue
50	Loss
60	
70	
80	
90	

REMARKS

[illegible]

WORKSHEET FOR CALCULATION OF STATIC COLUMN WELLHEAD PRESSURE (P_w)

Form C-122D
Adopted 9-1-65

COMPANY Gulf Oil Corporation LEASE Eddy GX State Comm. WELL NO. # 1 DATE 8/11/78

LOCATION: Unit 6694 Section 18 Township 18 Range 25

L 6694 H 6694 L/H 1.000 G mix .703 % CO₂ % N₂ % H₂S

d 1.995 F_r .018231 GH 4706 P_{cr} 668 T_{cr} 392
1st 2nd 3rd 4th

LINE	1st	2nd	1st	2nd	1st	2nd	1st	2nd		
1 Q _m	.472	.472	.686	.686	.967	.967	1.376	1.376		
2 T _w (W.H. °R)	534	534	534	534	534	534	534	534		
3 T _s (B.H. °R)	601	601	601	601	601	601	601	601		
4 T = ($\frac{1}{2}T_w + T_s$)	567.5	567.5	567.5	567.5	567.5	567.5	567.5	567.5		
5 Z (Est.)	.759	.747	.769	.756	.790	.775	.864	.850		
6 TZ	430.7	423.9	436.4	429.0	448.3	439.8	490.3	482.4		
7 GH/TZ	10,926	11,101	10,783	10,969	10,497	10,700	9,598	9,756		
8 e ^s (Table XIV)	1.506	1.516	1.498	1.509	1.482	1.494	1.433	1.442		
9 1-e ^s (Table XIV)	.336	.341	.333	.337	.325	.331	.302	.306		
10 P _t	1758.2	1758.2	1628.2	1628.2	1413.2	1413.2	838.2	838.2		
11 P _t ² /1000	3091.3	3091.3	2651.0	2651.0	1997.1	1997.1	702.6	702.6		
12 F _t (Table XV)	.018231	.018231	.018231	.018231	.018231	.018231	.018231	.018231		
13 F _c = F _t TZ	7.853	7.729	7.956	7.822	8.173	8.018	8.939	8.794		
14 F _c Q _m	3.71	3.65	5.46	5.37	7.90	7.75	12.30	12.10		
15 L/H (F _c Q _m) ²	13.7	13.3	29.8	28.8	62.5	60.1	151.3	146.4		
16 F _w = L/H (F _c Q _m) ² (1-e ^{-s})	4.62	4.53	9.91	9.71	20.33	19.87	45.73	44.36		
17 P _w ² = P _t ² + F _w	3095.9	3095.8	2660.9	2660.7	2017.5	2017.0	748.3	747.4		
18 P _s ² = e ^s P _w ²	4663.6	4694.2	3987.1	4014.6	2990.6	3012.8	1072.5	1077.6		
19 P _s	2159.5	2166.6	1996.8	2003.6	1729.3	1735.7	1035.6	1038.1		
20 P = ($\frac{P_t + P_s}{2}$)	1958.9	1962.4	1812.5	1815.9	1571.3	1574.5	936.9	938.1		
21 P _r = (P/P _{cr})	.2.93	.2.94	.2.71	.2.72	.2.35	.2.36	1.40	1.40		
22 T _r = (T/T _{cr})	1.45	1.45	1.45	1.45	1.45	1.45	1.45	1.45		
23 Z (Table XI)	.747	.747	.756	.755	.775	.774	.850	.850		