

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPO AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

0.5 F
122 file
RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 6-7-80		JUN 18 1980	
Company JAKE L. HAMON ✓				Location LLANO			
Pool TURKEY TRACK NORTH				MORROW		Unit O. C. D.	
Completion Date 6-4-80				Total Depth 11,000		Packer Set At 10,926	
Elevation 10,926				Final or Lease Name STATE LG 2895			
Csg. Size 5 1/2	Wt. 17.00	d 4.892	Set At 10,999	Perforations: From 10,862 To 10,884		Well No. 1	
Tbg. Size 2 7/8	Wt. 6.40	d 2.875	Set At 10,780	Perforations: From OPEN To END		Unit Sec. Twp. Rge. K 26 18S 28E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At 10,780		County EDDY	
Producing Thru TUBING		Reservoir Temp. °F 183 @ 10,894		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2	
State NEW MEXICO							
L 10,894	H 10,894	Gg .632	% CO ₂ .698	% N ₂ .427	% H ₂ S	Prover	Meter Run 4"
						Taps FLANGE	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1.	4 X 1.500			750	5	79	2661				45 MIN.
2.	4 X 1.500			765	12	72	2337				1 HR.
3.	4 X 1.500			770	19	69	2032				1 HR.
4.	4 X 1.500			775	28	68	1705				1 HR.
5.							1332				

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	10.84	61.77	763.2	.9822	1.258	1.067	883
2	10.84	96.64	778.2	.9887	1.258	1.070	1394
3	10.84	121.99	783.2	.9915	1.258	1.073	1770
4	10.84	148.56	788.2	.9924	1.258	1.076	2163
5							

NO.	P _t	Temp. °R	T _r	Z	Gas-Liquid Hydrocarbon Ratio	Mcf/bbl.
1	1.14	539	1.46	.878	71.710	
2	1.16	532	1.45	.873	A.P.I. Gravity of Liquid Hydrocarbons 54.8 @ 60°	
3	1.17	529	1.44	.869	Specific Gravity Separator Gas .632	X X X X X X X X
4	1.18	528	1.43	.863	Specific Gravity Flowing Fluid X X X X X	
5					Critical Pressure 670 P.S.I.A.	P.S.I.A.
					Critical Temperature 368 R	R

* $P_c = 2842.3$ $P_c^2 = 8078.7$

NO.	P_t^2	P_w^2	$P_w^2 - P_c^2$	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$
1	* 2528.1	6391.3	1687.4	1.383	1.294
2	* 2175.3	4731.9	3346.8		
3	* 1869.6	3495.4	4583.3		
4	* 1496.1	2238.3	5840.4		
5					

$\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.799$

Absolute Open Flow	2,799	Mcf/d @ 15.025	Angle of Slope θ	51.5	Slope, n	.795
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Remarks: **3.48 BBLs. OF FLUID**
*CALCULATED FROM KNOWN BHP

Approved By Commission:	Conducted By: W.S.	Calculated By: R.R.	Checked By: J.W.W.
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