

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT, ONE POINT BACK PRESSURE TEST FOR GAS WELL

C. S. F.
Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date <u>5-12-80</u>		MAY 16 1980	
Company <u>Anadarko Prod. Co.</u>		Connection <u>To Air</u>		O. C. D.	
Pool <u>N. Turkey Track morrow</u>		Formation <u>Morrow</u>		ARTESIA, OFFICE	
Completion Date <u>5-12-80</u>		Total Depth <u>11,150</u>		Plug back To <u>11,052</u>	
Casing Size <u>4 1/2</u>		Set At <u>11,110</u>		Perforations: From <u>10,871</u> To <u>10,888</u>	
Tubing Size <u>2 3/8</u>		Set At <u>10,845</u>		Perforations: From _____ To _____	
Type well - Single - Provenhead - G.G. or G.O. Multiple <u>Single</u>		Packer Set At <u>10,845</u>		State or Lease Name <u>State A C Com.</u>	
Producing thru <u>Tbg.</u>		Reservoir Temp. °F <u>183 @ 10,879</u>		Mean Annual Temp. °F <u>60</u>	
Baro. Press. - P _a <u>13.2</u>		County <u>Eddy</u>		State <u>New Mexico</u>	
L <u>10,879</u>	H <u>10,879</u>	G _g <u>.640</u>	% CO ₂	% N ₂	% H ₂ S
Prover		Meter Run <u>4</u>		Type <u>F1g</u>	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
51							2820				91 hrs.
1.	4	X	1.500	300	11	92	2544	76			1 hr
2.	4	X	1.500	300	20	90	2407	76			1 hr
3.	4	X	1.500	300	40	80	2055	75			1 hr
4.	4	X	1.500	300	77	89	1535	74			1 "
5.	4	X	2.00	300	29	87	977				1 "

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super. Factor, F _{sp}	Rate of Flow Q, Mld
1	10.84	58.70	313.2	.9706	1.250	1.026	792
2	10.84	79.15	313.2	.9723	1.250	1.026	1070
3	10.84	111.93	313.2	.9813	1.250	1.028	1530
4	10.84	155.29	313.2	.9732	1.250	1.026	2101
5	19.81	95.30	313.2	.9750	1.250	1.027	2362

NO.	η	Temp. °R	T_r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1	.47	552	1.48	.950	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2	.47	550	1.48	.950	Specific Gravity Separator Gas <u>.640</u> _____ X X X X X X X X
3	.47	540	1.45	.946	Specific Gravity Flowing Fluid _____ X X X X X
4	.47	549	1.48	.950	Critical Pressure <u>670</u> _____ P.S.I.A. _____ P.S.I.A.
5	.47	547	1.47	.948	Critical Temperature <u>372</u> _____ R _____ R

NO.	P_c^2	P_w^2	$P_c^2 - P_w^2$	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$
1	2662.6	7089.4	1747.5	1.195	1.146
2	2528.9	6395.3	2441.6		
3	2171.0	4713.2	4123.7		
4	1676.0	2809.0	6027.9		
5	1200.5	1441.2	7395.7		

AOR = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.709$

Post-1
ID 2 +
1000 ft
1000 ft

Absolute Open Flow <u>2,709</u> Mld @ 15.025	Angle of Slope <u>52.5</u>	Slope, n <u>.767</u>
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Remarks: Calculated from known bottom hole pressures.

Approved By Commission:	Conducted By: <u>B. R. Duke</u>	Calculated By: <u>Reggie Reston</u>	Checked By:
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