

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 8/20/81		SEP 8 1981	
Company Amoco Production Company				Connection Llano, Inc.			
Pool Scoggin Draw Morrow				Formation Morrow		Unit O. C. D. ARTESIA, OFFICE	
Completion Date 2/16/81		Total Depth 9880.		Plug Back TD 9640.		Elevation 3510.	
Csg. Size 5.500		Wt. 15.5		Set At 4.950		Perforations: From 9560. To 9661.	
Tbg. Size 2.375		Wt. 4.6		Set At 1.995		Perforations: From 0. To 0.	
Type Well - Single - Dradhead - G.C. or G.O. Multiple Single				Packer Set At 9460'		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 149. @ 9610.		Mean Annual Temp. °F 60.0		Baro. Press. - P _a 13.2	
L 9610.		H 9610.		G _g 0.664		% CO ₂ 0.62	
				% N ₂ 0.62		% H ₂ S 0.	
				Prover 0.		Meter Run 3.0	
						Taps Flange	

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	
1.	3.00 x 0.625			605.	9.0	78.	1760.	77.	4.2
2.	3.00 x 0.625			605.	21.0	78.	1706.	80.	1.0
3.	3.00 x 0.625			600.	46.0	81.	1617.	80.	1.0
4.	3.00 x 0.625			595.	85.0	80.	1464.	81.	1.0
5.									1.0

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	1.85	74.59	618.2	0.9831	1.2273	1.0584	176.
2.	1.85	113.94	618.2	0.9831	1.2273	1.0584	269.
3.	1.85	167.95	613.2	0.9804	1.2273	1.0568	395.
4.	1.85	227.37	608.2	0.9813	1.2273	1.0567	535.
5.							

NO.	P _t	Temp. °R	T _g	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	0.92	538.	1.43	0.893	0.	0.	0.664	XXXXXX	671.	376.
2.	0.92	538.	1.43	0.893				XXXXXX		
3.	0.91	541.	1.44	0.895						
4.	0.91	540.	1.44	0.896						
5.										

P _c 1853.2 P _c ² 3434.					$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{2.6579}{\quad}$		$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{2.2619}{\quad}$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1210.}{\quad}$			
1.	3144.	1756.	3085.	349.				
2.	2956.	1701.	2892.	542.				
3.	2658.	1614.	2604.	830.				
4.	2182.	1464.	2142.	1292.				
5.								

Absolute Open Flow 1210. Mcfd @ 15.025		Angle of Slope θ 49.6	Slope, n 0.851
Remarks:			
Approved By Commission:		Conducted By: John West Engr.	Calculated By: D. Etheridge
		Checked By: L. W. Sheppard	