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appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator OXY USA INC.					Lease or Unit Name MUSTANG ST. COM.				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 6-MAY-97		Well No. 1		
Completion Date		Total Depth		Plug Back TD		Elevation		Unit Ltr. - Sec. - TWP - Rge. I-16-18S-29E	
Csg. Size	Wt.	d	Set At	Perforations: From: 10,656 To: 10,686		County EDDY			
Tbg. Size	Wt.	d	Set At	Perforations: From: To:		Pool			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple					Packer Set At 10,578		Formation		
Producing Thru		Reservoir Temp. °F 161		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2		Connection	
L 10,671	H 10,671	Gg 0.642	% CO ₂ 0.26	% N ₂ 1.08	% H ₂ S 0	Prover		Meter Run 4.0	Taps FLANGE

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI									1989	161	92.5
1.	4.00	X	0.75	1388	10.5	105	--	--	1814	161	1
2.	4.00	X	0.75	1250	23.1	105	--	--	1736	161	1
3.	4.00	X	0.75	1134	32.8	96	--	--	1633	161	1
4.	4.00	X	0.75	945	55.0	72	--	--	1390	161	1
5.											

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.		121.27	1400.7	0.9594	1.2481	1.0971	620
2.		170.82	1263.2	0.9591	1.2481	1.0888	905
3.		193.95	1146.9	0.9674	1.2481	1.0879	1160
4.		229.56	958.2	0.9891	1.2481	1.0897	1739
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio 108.4 Mcf/bbl.		
1.	2.09	565	1.53	0.831	A.P. I. Gravity of Liquid Hydrocarbons 54.4 Deg.		
2.	1.89	565	1.54	0.844	Specific Gravity Separator Gas 0.642 XXXXXXXXXX		
3.	1.71	556	1.51	0.845	Specific Gravity Flowing Fluid XXXXX 0.667		
4.	1.43	532	1.44	0.842	Critical Pressure 670 P.S.I.A. 668 P.S.I.A.		
5.					Critical Temperature 368 R 376 R		

P _c 1489.0		P _c ² 2217				
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{2.0246}{1}$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1.8668}{1}$
1.	3339	1364	1862	356	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{3246}{1}$	
2.	3059	1309	1713	505		
3.	2710	1235	1525	693		
4.	1969	1059	1122	1095		
5.						

Absolute Open Flow 3246 Mcfd @ 15.025	Angle of Slope Θ 48.5	Slope, n 0.885
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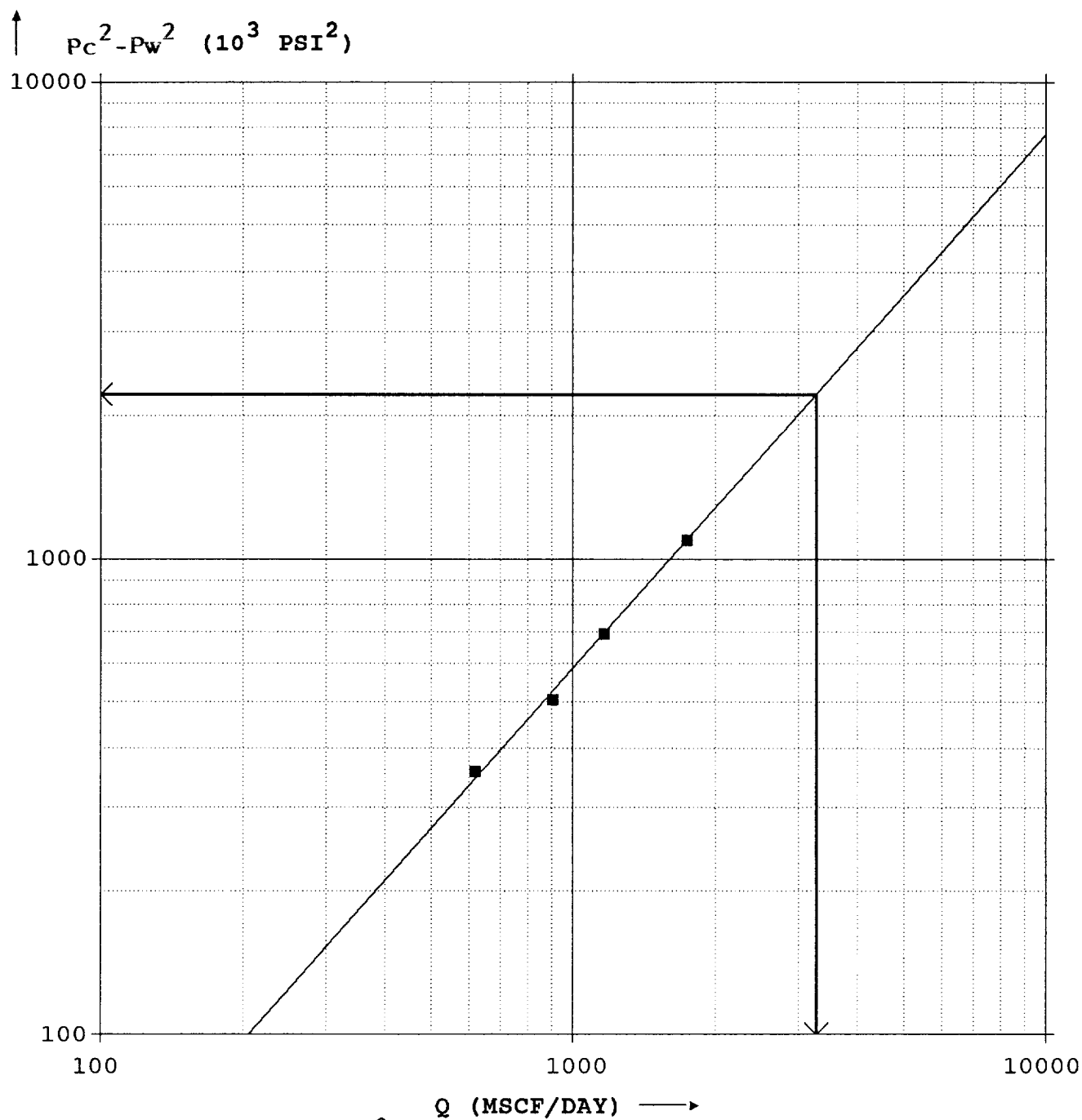
Remarks: BASED ON BOTTOM HOLE PRESSURE MEASUREMENTS

Approved By Division	Conducted By: <i>Harry Davis by RHA</i>	Calculated By: <i>Michael Lyle Beckhammer</i>	Checked By:
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BACK PRESSURE CURVE

CLIENT: OXY USA
WELL: MUSTANG ST. COM. #1

Test Date: 06-MAY-1997
County: EDDY, NM



Well Tester: Larry Davis by [Signature]
SCHLUMBERGER Testing

θ = 48.235 degrees
 n = 0.8930
AOF = 3264.0 MSCF/DAY