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See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

RECEIVED
ARTESIA

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator OXY USA INC.					Lease or Unit Name COLT FEDERAL				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 9-FEB-1998				
Completion Date 12-JAN-1998					Well No. 1				
Total Depth 11,420					Plug Back TD 10,721				
Elevation 3499					Unit Ltr. - Sec. - TWP - Rge. 9 - 18S - 29E				
Csg. Size 4.5		Wt. 11.6		Set At 10,643		Perforations: From: 10,721 To: 10,740		County EDDY	
Tbg. Size 2 3/8		Wt. 4.7		Set At 10,643		Perforations: From: To:		Pool MORROW	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE					Packer Set At 10,643				
Producing Thru TUBING 160					Baro. Press - P 13.2				
Reservoir Temp. °F 60					Formation MORROW				
Mean Annual Temp. °F 60					Connection CONOCO PIPELINE				
L 10,730		H 10,730		Gg 0.652		% CO ₂ 0.46		% N ₂ 1.18	
				% H ₂ S 0		Prover 4.0		Meter Run 4.0	
								Taps FLANGE	

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1.	4.03 X 2.0		182	13.8	68	1908*	60*	2755	160	69.0
2.	4.03 X 2.0		193	24.6	79	1875*	60*	2647	160	0.8
3.	4.03 X 2.0		210	47.8	73	1775*	60*	2617	160	0.8
4.	4.03 X 2.0		174	74.7	65	1613*	60*	2526	160	0.8
5.								2416	160	0.8

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _L	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.		51.86	194.9	0.9924	1.2384	1.0181	1367
2.		71.22	206.2	0.9819	1.2384	1.0178	1767
3.		103.22	222.9	0.9877	1.2384	1.0201	2551
4.		118.10	186.7	0.9955	1.2384	1.0177	3402
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P. I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	0.29	528	1.42	0.965	0	0	0.652	XXXXXX	670	371
2.	0.31	539	1.45	0.965						
3.	0.33	533	1.44	0.961						
4.	0.28	525	1.42	0.966						
5.										

P _c 2062.4 P _c ² 4253					$1) \frac{P_c^2}{P_c^2 - P_w^2} = 4.3894$		$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3.2050$	
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²				
1.	7079	1982	3930	324				
2.	6918	1960	3841	412				
3.	6445	1893	3582	671				
4.	5900	1812	3284	969				
5.								

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 10,903$				
Absolute Open Flow 10,903 Mcfd @ 15.025 Angle of Slope θ 51.8 Slope, n 0.787				

Remarks: **CALCULATIONS BASED ON BOTTOM HOLE PRESSURE**

***FOR REFERENCE ONLY, NOT USED IN CALCULATIONS**

Approved By Division	Conducted By: <i>Harry Davis by G.A.</i>	Calculated By: <i>Whitely Prokammer</i>	Checked By:
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