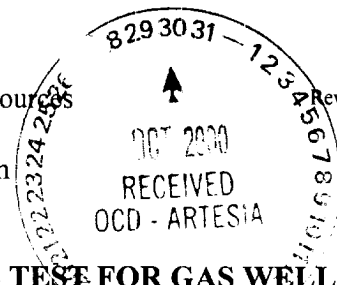


Submit in duplicate to
appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources

Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

Form C-122
Revised October, 1999



CISF

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator Fasken Oil and Ranch, Ltd.					Lease or Unit Name Yates Federal				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 10-6-00		Well No. 3		
Completion Date 10-4-00		Total Depth 8,700'		Plug Back TD 8,620'		Elevation 3423'		Unit Ltr. - Sec. - TWP - Rge. F 6 18S 26E	
Csg. Size 4-1/2"	Wt. 11.6	d 4.000	Set At 8,699'	Perforations: From: 8460' To: 8492'				County Eddy	
Tbg. Size 2-7/8"	Wt. 4.7	d 2.441	Set At 8,420'	Perforations: From: To:				Pool East Eagle Creek	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single					Packer Set At 8,420'		Formation Morrow		
Producing Thru Tubing		Reservoir Temp. °F 134		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2		Connection El Paso Energy Services	
L 8420	H 8420	G _g 0.60	%CO ₂ 0.8	%N ₂ 0.20	%H ₂ S 0.00	Prover	Orifice	Meter Run 2"	Taps Flange

FLOW DATA					TUBING DATA		CASING DATA		Duration Of Flow	
No.	Prover Line Size	Orifice X Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1.		2.067" x 0.75"	450	11.6	90	450	90	0		22 hr
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS							
No.	COEFFICIENT (24 HOUR)	$\frac{V}{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	2.941	73.26	463.2	0.9723	1.291	1.039	281
2.							
3.							
4.							
5.							

No.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	0.69	550	1.47	0.926	A. P. I. Gravity of Liquid Hydrocarbons	Deg.
2.					Specific Gravity Separator Gas 0.6	XXXXXXXXXX
3.					Specific Gravity Flowing Fluid 0.6	XXXXXX
4.					Critical Pressure 674	P.S.I.A. P.S.I.A.
5.					Critical Temperature 357	R. R.

P _c 1688.2		P _c ² 2850.0	
No.	P _i ²	P _w	P _w ²
1.	202.5	463.2	214.6
2.			
3.			
4.			
5.			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{2850.0}{2635.4}$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0814$

AOF = Q (281) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 304$

Absolute Open Flow 304	Mcf/d @ 15.025	Angle of Slope θ: 45	Slope, n: 1.0
Remarks:			
Approved By Division	Conducted By: Fasken Oil and Ranch, Ltd.	Calculated By: Carl Brown	Checked By: