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appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources

Form C-122
Revised October, 1999

Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505



CLSF

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator Fasken Oil and Ranch, Ltd.					Lease or Unit Name Yates "6" Federal				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 10-22-00		Well No. 3		
Completion Date 10-4-00		Total Depth 8,700'		Plug Back TD 8,620'		Elevation 3423'		Unit Ltr. - Sec. - TWP - Rge. F 6 18S 26E	
Csg. Size 4-1/2"	Wt. 11.6	d 4.000	Set At 8,699'	Perforations: From: 8036' To: 8078'				County Eddy	
Tbg. Size 2-3/8"	Wt. 4.7	d 1.995	Set At 8,420'	Perforations: From: To:				Pool Eagle Creek	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 8,420'		Formation Strawn			
Producing Thru Tubing		Reservoir Temp. °F 130		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2		Connection El Paso Energy Services	
L 8416	H 8416	Gg 0.638	%CO ₂ 0.27	%N ₂ 0.60	%H ₂ S 0.00	Prover Orifice	Meter Run 2"	Taps Flange	

FLOW DATA					TUBING DATA		CASING DATA		Duration Of Flow
No.	Prover Line Size	Orifice X Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI						1440	75	0	
1.	2.067" x 0.75"		510	2.27	90	510	90	0	
2.									
3.									
4.									
5.									

RATE OF FLOW CALCULATIONS							
No.	COEFFICIENT (24 HOUR)	h _w P _m	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F pv.	Rate of Flow Q, Mcfd
1.	2.941	34.46	523.2	0.9723	1.265	1.043	130
2.							
3.							
4.							
5.							

No.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	0.76	550	1.47	0.919	A. P. I. Gravity of Liquid Hydrocarbons	Deg.
2.					Specific Gravity Separator Gas 0.638	XXXXXXXXXX
3.					Specific Gravity Flowing Fluid 0.638	XXXXXX
4.					Critical Pressure 670	P.S.I.A.
5.					Critical Temperature 372	R.

P _c 1453.2		P _c ² 2111.8	
No.	P _r ²	P _w	P _w ²
1.	260.1	463.2	273.7
2.			
3.			
4.			
5.			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{2111.8}{1838.1}$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.1489$

AOF = Q (130) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 149$

Absolute Open Flow 149	Mcf/d @ 15.025	Angle of Slope θ: 45	Slope, n: 1.0
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Remarks: Tubing has sliding sleeve open at 8416', 4 feet above packer.

Approved By Division	Conducted By: Fasken Oil and Ranch, Ltd.	Calculated By: Carl Brown	Checked By:
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