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NEW MEXICO OIL CONSERVATION COMMISSION

FEB 9 1960

Corrected Report

Form C-122

O. C. C. Revised 12-1-55

ARTESIA, OFFICE

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool **Shugart-Penn** Formation **Pennsylvanian** County **Eddy**

Initial **X** Annual _____ Special _____ Date of Test **1-12&13-60**

Company **Continental Oil Company** Lease **Greenwood Unit** Well No. **6**

Unit **J** Sec. **26** Twp. **18-S** Rge. **31-E** Purchaser _____

Casing **5½"** Wt. **20#** I.D. **4892** Set at **12,052** Perf. **11,220 / 11,381** To **11,225 / 11,390**

Tubing **2 3/8"** Wt. **4.7#** I.D. **2.041** Set at **11,170** Perf. **11,530** To **11,533**

Gas Pay: From **11,220 / 11,381** To **11,225 / 11,390** L _____ xG _____ -GL _____ Bar.Press. **13.2**

Producing Thru: Casing _____ Tubing **X** Type Well **Single**
Single-Bradenhead-G. G. or G.O. Dual

Date of Completion: **1-14-60** Packer **Guiberson - 11,170** Reservoir Temp. **142**

OBSERVED DATA

Tested Through (Prover) (Choke) (Meter) **Orifice Well Tester** Type Taps _____

No.	Flow Data (Prover) (Line) Size	Flow Data (Choke) (Orifice) Size	Flow Data Press. psig	Flow Data Diff. h_w	Flow Data Temp. °F.	Tubing Data Press. psig	Tubing Data Temp. °F.	Casing Data Press. psig	Casing Data Temp. °F.	Duration of Flow Hr.
SI	2"	1"				2245	-	Packer	-	21 hr. SI
1.	2"	1"	23#		60	67	-	"	-	7 hrs.
2.	2"	1"	20#		60	113	-	"	-	4 hrs.
3.	2"	1"	18#		60	180	-	"	-	5 hrs.
4.	2"	3/4"	36#		60	350	-	"	-	6 hrs.
5.										

FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_w p_f}$	Pressure psia	Flow Temp. Factor F_t	Gravity Factor F_g	Compress. Factor F_{pv}	Rate of Flow Q-MCFPD @ 15.025 psia
1.					.9359		696.0
2.					.9359		639.7
3.					.9359		597.2
4.					.9359		509.0
5.							

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio **12,500** cf/bbl. Specific Gravity Separator Gas **.683**

Gravity of Liquid Hydrocarbons **50.7** deg. Specific Gravity Flowing Fluid **.888**

P_c _____ $(1-e^{-s})$ _____ P_c **2258.2** P_c^2 **5099.5**

No.	P_w * P_t (psia)	P_t^2	F_cQ	$(F_cQ)^2$	$\frac{(F_cQ)^2}{(1-e^{-s})}$	P_w^2	$P_c^2-P_w^2$	Cal. P_w	$\frac{P_w}{P_c}$
1.	80.2					6.4	5093.0		.0357
2.	126.2					15.9	5083.5		.0562
3.	193.2					37.3	5062.1		.0861
4.	363.2					131.9	4967.6		.1618
5.									

Absolute Potential: **700** MCFPD; n **10.7**

COMPANY **CONTINENTAL OIL COMPANY**

ADDRESS **Rowley Building, Artesia, New Mexico**

AGENT and TITLE **L. W. Bingham, Test Engineer**

WITNESSED **L. Duncan**

COMPANY **Continental Oil Company**

REMARKS

***Stabalized tubing pressure taken with Dead Weight Tester**

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

Q = Actual rate of flow at end of flow period at W. H. working pressure (P_w). MCF/da. @ 15.025 psia and 60° F.

P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia

P_w = Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia

P_t = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

P_f = Meter pressure, psia.

h_w = Differential meter pressure, inches water.

F_g = Gravity correction factor.

F_t = Flowing temperature correction factor.

F_{pv} = Supercompressability factor.

n = Slope of back pressure curve.

Note: If P_w cannot be taken because of manner of completion or condition of well, then P_w must be calculated by adding the pressure drop due to friction within the flow string to P_t.