OPERATOR'S COPY

FORM 1016
(1970)

OKLAHOMA CORPORATION COMMISSION – OIL & GAS CONSERVATION DIVISION
BACK – PRESSURE TEST FOR NATURAL GAS WELLS

TYPE TEST: ☐ INITIAL ☐ ANNUAL ☒ SPECIAL	TEST DATE 1-23-71			OKLAHOMA TAX COMMISSION ASSIGNED LEASE NO.
COMPANY Roger C. Hanks	CONNECTION None			
FIELD Indian Basin	ALLOCATED POOL NO.	RESERVOIR Cisco Canyon	LOCATION	UNIT
COMPLETION DATE	TOTAL DEPTH 7801	PLUG BACK TD 7767	ELEVATION 3698 + 16'	FARM OR LEASE NAME Preston
CSG. SIZE 7"	WT. 23-26	d	SET AT 7801	PERFORATIONS: FROM TO 7668 - 7700
TBG. SIZE 2-3/8	WT. 4.7	d 1.995	SET AT 7576	PERFORATIONS: FROM TO
TYPE COMPLETION (DESCRIBE) Single			PACKER SET AT	WELL NO. 1
PRODUCING THRU Tubing	RESERVOIR TEMP. F 143 @ 7684	MEAN GROUND TEMP. F 74	BARO. PRESS.– P_a 14.4	SEC. 35 TWP– 20S RGE– 24 ECM
				COUNTY Eddy
				STATE New Mexico

L	H	G_g	% CO_2	% N_2	% H_2S	PROVER	METER RUN	TAPS
7684	7684	.650	.63	.82	.28		4.026	Flg.

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	(~~PROVER~~) (LINE) X ORIFICE SIZE SIZE	PRESS. PSIG	DIFF. (INCHES) (~~METER~~)	TEMP. F	PRESS. PSIG	TEMP. F	PRESS. PSIG	TEMP. F	DURATION OF FLOW, HR.
SI									
1.	4 x 1.250	171.0	59	85	445	90			96
2.	4 x 1.250	171.0	50	85	485	90			1
3.	4 x 1.250	171.0	30	85	633	90			1
4.	4 x 1.250	171.0	21	85	719	89			1
5.									

RATE OF FLOW CALCULATIONS

NO.	COEFFICIENT (24-HOUR)	$\sqrt{h_w P_m}$	PRESSURE P_m	FLOW TEMP. FACTOR, F_t	GRAVITY FACTOR, F_g	SUPER COMPRESS. FACTOR, F_{pv}	RATE Q, MCFPD
1.	~~7.857~~ 7.711	104.2	184.2	.9768	1.240	1.016	~~1008~~
2.	~~7.857~~	96.0	184.2	.9768	1.240	1.016	928
3.	~~7.857~~	74.3	184.2	.9768	1.240	1.016	718
4.	~~7.857~~	62.2	184.2	.9768	1.240	1.016	~~601~~
5.							

NO.	P_r	TEMP. R	T_r	Z
1.	.27	545	1.45	.969
2.	.27	545	1.45	.969
3.	.27	545	1.45	.969
4.	.27	545	1.45	.969
5.				

GAS LIQUID HYDROCARBON RATIO 840 MCF/BBL
API GRAVITY OF LIQUID HYDROCARBONS 61.0 DEG.
SPECIFIC GRAVITY SEPARATOR GAS .650 XXXXXXXXX
SPECIFIC GRAVITY FLOWING FLUID XXXX .650
CRITICAL PRESSURE 670 PSIA 670 PSIA
CRITICAL TEMPERATURE 375 R 375 R

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O. C. C.
ARTESIA, OFFICE

P_c 2400 * P_c^2 5760

NO.	P_w	P_w^2	$P_c^2 - P_w^2$
1.		236.6	5523.4
2.		270.7	5489.3
3.		430.7	5329.3
4.		545.1	5214.9
5.			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = $ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$

WHAOF = $Q\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$

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ARTESIA, NEW MEXICO

CALCULATED WELLHEAD OPEN FLOW 1,080 MCFD @ ~~15.025~~ ANGLE OF SLOPE θ 45.0 SLOPE, n 1.000

REMARKS: * Calculated wellhead pressure after 72 hours
Well producing fluid rate: 56 BBl. H_2O/hour
0.05 BBl. 61° API Cond/hour

APPROVED BY COMMISSION:	CONDUCTED BY:	CALCULATED BY:	CHECKED BY: