

N MEXICO OIL CONSERVATION COMM. ON
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS

Form C-122
Revised 9-1-65

FEB 8 1972

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 2-2-72			
Company HANAGAN PETROLEUM CORP. /				Connection NONE		O. C. C. ARTESIA, OFFICE	
Pool WC UNDESIGNATED				Formation MORROW		Unit	
Completion Date 2-4-72		Total Depth 11050		Plug Back TD 10994		Elevation 3550 KB	
Farm or Lease Name MILLMAN DEEP							
Csg. Size 4 1/2	Wt. 11.6	d 4.000	Set At 11050	Perforations: From 10876 To 94		Well No. 1	
Tbg. Size 2 3/8	Wt. 4.7	d 1.995	Set At 10520	Perforations: From To		Unit Sec. Twp. Rge. B 4 19S 28E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At 10520-25		County EDDY	
Producing Thru TBG		Reservoir Temp. °F 168 @ 10485		Mean Annual Temp. °F		State NEW MEXICO	
L 10885	H 10885	Gg 0.600	% CO ₂	% N ₂	% H ₂ S	Prover Pos. Ck.	Meter Run Taps

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI				2817			2817		Pkr.		
1.	2"	X	8/64"	2644		70	2644	70	"		60 min.
2.	2"	X	10/64"	2561		71	2561	71	"		60 min.
3.	2"	X	13/64"	2216		72	2216	72	"		60 min.
4.	2"	X	16/64"	1975		73	1975	73	"		60 min.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	0.2618		2657.2	0.9905	1.291	1.145	1018.5
2	0.4173		2574.2	0.9896	1.291	1.146	1572.8
3	0.7208		2229.2	0.9887	1.291	1.143	2344.2
4	1.1120		1988.2	0.9877	1.291	1.138	3208.2
5							

NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	Dry Gas	Mcf/bbl.
1	3.96	530	1.48	0.763	A.P.I. Gravity of Liquid Hydrocarbons	None	Deg.
2	3.84	531	1.48	0.761	Specific Gravity Separator Gas	0.600	XXXXXXX
3	3.32	532	1.49	0.766	Specific Gravity Flowing Fluid	XXXXX	
4	2.96	533	1.49	0.772	Critical Pressure	671	P.S.I.A.
5					Critical Temperature	358	P.S.I.A.

NO.	P _f	P _s	P _s ²	P _f ² - P _s ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$
1	3764.2	14169	3548.2	12590	1579	
2			3437.2	11814	2355	
3			3030.2	9182	4987	
4			2756.2	7597	6572	
5						

Absolute Open Flow				Angle of Slope		Slope, n	
6400 Mcfd @ 15.025				500 52'		0.81354	

Remarks: BHP measured with Amerada RPG-3 gauge.

Approved By Commission:	Conducted By: Tefteller, Inc.	Calculated By: F. Tefteller	Checked By:
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