

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

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Type Test ☐ Initial ☐ Annual ☒ Special			Test Date 7-24-73		SEP 11 1973		
Company Hanagan Petroleum Corp.			Connection				
Pool Millman Deep			Formation Morrow			Unit B	
Completion Date 2-4-72		Total Depth 11050		Plug Back TD 10994		Elevation 3550 KB	
Farm or Lease Name Millman Deep			Well No. 1				
Csg. Size 4 1/2	Wt. 11.6	d 4.000	Set At 11050	Perforations: From 10876 To 10894		Unit Sec. Twp. Rge. B 4 19S 28E	
Tbg. Size 2 3/8	Wt. 4.7	d 1.995	Set At 10520	Perforations: From To			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 10520-25		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 168 @ 10485		Mean Annual Temp. °F 70		State New Mexico	
L 10885	H 10885	Gg 0.600	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run X
Taps							

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							1975				
1.	4"	X	1"	795	9	63	1866	70			60 min.
2.	4"	X	1"	795	18	61	1787	70			60 min.
3.	4"	X	1"	795	39	61	1704	70			60 min.
4.	4"	X	1"	795	81	62	1531	70			60 min.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	4.753	85.29	808.2	0.9971	1.291	1.072	559.4
2	4.753	120.61	808.2	0.9990	1.291	1.072	792.6
3	4.753	177.54	808.2	0.9990	1.291	1.072	1166.7
4	4.753	255.86	808.2	0.9981	1.291	1.072	1679.8
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Dry Gas	Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons	None	Deg.
2.	Simplified Supercompressibility Tables Uses				Specific Gravity Separator Gas	0.600	X X X X X X X X
3.					Specific Gravity Flowing Fluid	X X X X X	
4.					Critical Pressure	671	P.S.I.A.
5.					Critical Temperature	358	R

P _f	2659.2	P _f ²	7071
NO.	P _t ²	P _s	P _s ²
1		2507.2	6286
2		2439.2	5950
3		2312.2	5346
4		2138.2	4572
5			

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{P_c^2}{P_c^2 - P_w^2}$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$$

Absolute Open Flow	4550	Mcf/d @ 15.025	Angle of Slope	46° 23'	Slope, n	0.95282
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Remarks: **BHP measured with Amerada RPG-3 gauge.**

Approved By Commission:	Conducted By: Teffteller, Inc.	Calculated By: F. Teffteller	Checked By:
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