

N MEXICO OIL CONSERVATION COMM JN
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

0-122

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 11-18-74		RECEIVED JAN 9 - 1975	
Company Read & Stevens, Inc				Connection Pending					
Pool Cemetary				Formation Morrow				Unit O. C. C.	
Completion Date 9-1-1974				Total Depth 9764		Plug Back TD 9710		Elevation 3507 GL	
Farm or Lease Name Mesa "Comm."				Well No. 1					
Csg. Size 5 1/2	Wt. 15 1/2-17	d 5	Set At 9764	Perforations: From 9585 To 9594					
Tbg. Size 2 3/8	Wt. 4.7	d 1.995	Set At 9526	Perforations: From NONE to Packer					
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 9526		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 165° 9500		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State N. Mexico	
L 9585	H 9585	G _g 0.5895	% CO ₂ 2.23	% N ₂ .40	% H ₂ S —	Prover —	Meter Run 3.068	Taps Flange	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	—	—	—	—	—	—	2281	—	—	—	16 1/2 hrs.
1.	3.068	—	1.0	370	4	116	2154	60	PKR	—	60
2.	3.068	—	1.0	370	17	105	2016	60	—	—	60
3.	3.068	—	1.0	380	28	104	1903	60	—	—	90
4.	3.068	—	1.0	380	39	98	1806	60	—	—	75
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	4.789	39.15	383.2	0.9501	1.302	1.021	236.8
2.	4.789	80.71	383.2	0.9594	1.302	1.023	493.9
3.	4.789	104.93	393.2	0.9602	1.302	1.023	642.7
4.	4.789	123.83	393.2	0.9653	1.302	1.024	763.2
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	0.562	576	1.646	0.960	—	—	0.5895	XXXXXX	682	350
2.	0.562	565	1.614	0.956	—	—	—	XXXXX	—	—
3.	0.577	564	1.611	0.955	—	—	—	—	—	—
4.	0.577	558	1.594	0.953	—	—	—	—	—	—
5.										

NO.	P _r ²	P _w *	P _w ²	P _r ² - P _w ²
1.	—	2956.2	8739.1	262.1
2.	—	2880.2	8295.6	705.6
3.	—	2782.2	7740.6	1260.6
4.	—	2717.2	7383.2	1618.0
5.				

(1) $\frac{P_r^2}{P_r^2 - P_w^2} =$ _____

AOF = Q $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n =$ _____

(2) $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n =$ _____

Absolute Open Flow 2350	Mcfd @ 15.025	Angle of Slope θ	Slope, n .641
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Remarks: *** BHP Bomb set @ 9590'**

Approved By Commission:	Conducted By: L. A. Owens	Calculated By: L. A. Owens	Checked By:
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