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C-122
Form C-122
Revised 9-1-65

NEW MEXICO OIL CONSERVATION COM. SION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 10-14-75		OCT 17 1975	
Company R.C. BENNETT & RYAN				Connection None					
Pool Wildcat Upper Perm. Winchester				Formation Cisco Canyon				Unit ARTESIA, DEPOSE	
Completion Date 10-14-75		Total Depth 11,360		Plug Back TD 11310		Elevation 3320 ft.		Farm or Lease Name Exxon St.	
Csq. Size 4 1/2	Wt. 11.6&13	d 11,360	Set At 11,360	Perforations: From 9692 To 10,003		Well No. 1			
Tbg. Size 2 3/8	Wt. 4.7	d 9,574	Set At 9,574	Perforations: From OPEN TO END		Unit Sec. Twp. Rge. N 25 19 28			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 9574		County Eddy	
Producing Thru TBG		Reservoir Temp. °F 171 @ 9692		Mean Annual Temp. °F 13.2		Baro. Press. - P _a 13.2		State N.M.	
L 9574	H 9574	Gg .712	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run 4"	Taps FLG	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	of Flow
SI							2287		S. I. P.		24 Hr.
1.	4	x	1.000	600	56	66	1083				1 Hr.
2.	4	x	1.000	600	28	69	1167				1 Hr.
3.	4	x	1.000	590	15	69	1265				1 Hr.
4.	4	x	1.000	580	7	68	1330				1 Hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	4.753	185.31	613.2	.9943	1.185	1.078	1,119
2	4.753	131.03	613.2	.9915	1.185	1.076	787
3	4.753	95.12	603.2	.9915	1.185	1.075	571
4	4.753	64.44	593.2	.9924	1.185	1.073	386
5.							

NO.	R _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	2.651	Mcf/bbl.
1.	.92	526	1.33	.860	A.P.I. Gravity of Liquid Hydrocarbons	49 @ 60	Deq.
2.	.92	529	1.34	.864	Specific Gravity Separator Gas	.712	X X X X X X X X
3.	.90	529	1.34	.866	Specific Gravity Flowing Fluid	X X X X X	G Mix = 1.633
4.	.89	528	1.34	.868	Critical Pressure	668	* P.S.I.A.
5.					Critical Temperature	395	* R

P _c 2300.2 P _c ² 5290.9						
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.307$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.307$
1			1243.8	4047.1		
2			1412.4	3878.5		
3			1643.9	3647.0		
4			1808.8	3482.1		
5						

Absolute Open Flow 1,462 Mcfd @ 15.025			Angle of Slope 45	Slope, n 1.000
Remarks: * A.O.F. calculated from Gr. of separator gas, due to Gmix being unreasonable.				
Approved By Commission:		Conducted By: R. Reston	Calculated By: J. B. Murray	Checked By: