

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

*Copy to SI-
C-122*

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Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 2-13-76			
Company Depco, Inc.				Connection		FEB 25 1976	
Pool Wildcat <i>monroe</i>				Formation Morrow		Unit O. C. C. ARTESIA, OFFICE	
Completion Date 1-28-76		Total Depth 11,553		Plug Back TD 11,055		Elevation 3503 KB	
Farm or Lease Name D H Y - State				Well No. 1			
Csg. Size 5 1/2	Wt. 17	d 4.892	Set At 11,411	Perforations: From 11,025 To 11,047			
Thq. Size 2 3/8	Wt. 4.7	d 2.375	Set At 11,048	Perforations: From To			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple G G Multiple				Packer Set At 8811		County Eddy	
Producing Thru Casing		Reservoir Temp. °F 185 @ 11,036		Mean Annual Temp. °F		Baro. Press. - P _a 13.2	
State New Mexico							
L 11,036	H 11,036	G _g .603	% CO ₂ Nil	% N ₂ Nil	% H ₂ S Nil	Prover	Meter Run X
						Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI									2860	73	
1.	3"	x	1.750	510	1.5	76			2510	66	1 hr.
2.	3"	x	1.750	517	9	65			2221	64	1 hr.
3.	3"	x	1.750	560	27	72			1870	67	1 hr.
4.	3"	x	1.750	545	49	64			1583	67	2 hrs.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	15.61	28.014	523.2	.9850	1.2878	1.041	577
2	15.61	69.078	530.2	.9952	1.2878	1.045	1,444
3	15.61	124.404	573.2	.9887	1.2878	1.046	2,586
4	15.61	167.062	558.2	1.0039	1.2878	1.049	3,536
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	115,462	Mcf/bbl.
1.	.78	536	1.50	.922	A.P.I. Gravity of Liquid Hydrocarbons	48.8	Deg.
2.	.79	525	1.47	.915	Specific Gravity Separator Gas	.603	X X X X X X X X
3.	.85	532	1.49	.914	Specific Gravity Flowing Fluid	X X X X X	.628
4.	.83	524	1.46	.909	Critical Pressure	671	P.S.I.A. 670
5.					Critical Temperature	358	R 368

P _c 2873.2	P _c ² 8255		
NO.	P _t ²	P _w	P _w ²
1	2524.3	6372	1883
2	2235.7	4998	3257
3	1886.0	3557	4698
4	1601.1	2564	5691
5			

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.4649$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 5217$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.4649$$

Absolute Open Flow	5,217	Mcf/d @ 15.025	Angle of Slope °	45	Slope, n	1.000
Remarks:						

Approved By Commission:	Conducted By: Tom Hanson Sonpany	Calculated By: Harrington	Checked By:
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MAR 12 1976

O. C. C.
ARTESIA, OFFICE