

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL
RECEIVED

3F
122 file
Form C-122
Revised 9-1-65
file

R-5609
1-1-78

Type Test ☒ Initial JUL 8 1977 ☐ Annual ☐ Special				Test Date 5-6-77	
Company O. C. C. ☒ Connection					
Yates Petroleum Corporation				El Paso Natural Pipeline Co.	
Pool <i>millman straw</i> Wildcat		Formation Strawn		Unit	
Completion Date 3-21-77		Total Depth 11152 KB		Plug Back TD 10602 KB	
				Elevation 3540 KB	
Farm or Lease Name N. Millman Unit					
Csg. Size 4 1/2"	Wt. 11.6#	d 4.000	Set At 10977 KB	Perforations: From 9792 To 9796 KB	
Tbg. Size 2-3/8"	Wt. 4.7#	d 1.995	Set At 9790 KB	Perforations: From 9741 To 9743	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 9734 KB	
Producing Thru Tubing		Reservoir Temp. °F 150° 9794		Mean Annual Temp. °F 62	
				Baro. Press. - P _a 13.2	
State New Mexico					
L .9780	H 9780	Gg	% CO ₂ 0.45	% N ₂ 1.83	% H ₂ S Nil
Prover		Meter Run 4"		Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2435	62			Weeks
1.	4.026 x 0.750			505	9	64	1846	68			1 hour
2.				507	16	66	1748	72			1 hour
3.				510	30	68	1610	75			1 hour
4.				512	56	70	1457	78			1 hour
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	2.661	68.29	518.2	.9962	1.193	1.0618	229
2.		91.23	520.2	.9943	1.193	1.0606	305
3.		125.28	523.2	.9924	1.193	1.0600	418
4.		171.51	525.2	.9905	1.193	1.0591	571
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio 15.137 Mcf/bbl.
1.	.775	524	1.354	.887	A.P.I. Gravity of Liquid Hydrocarbons 56.3 Deg.
2.	.778	526	1.359	.889	Specific Gravity Separator Gas 0.703 X X X X X X X X
3.	.782	528	1.364	.890	Specific Gravity Flowing Fluid X X X X X 0.886
4.	.785	530	1.370	.8915	Critical Pressure 669 P.S.I.A. 663 P.S.I.A.
5.					Critical Temperature 387 R 447 R

F _c 3722.6 P _c ² 13857				
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1			8674	5183
2			7868	5989
3			6749	7108
4			5564	8293
5				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.6709$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 954 \text{ MCFPD}$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.6709$$

Absolute Open Flow 954 Mcfd @ 15.025	Angle of Slope 45°	Slope, n 1.000
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Remarks: **Pressures by DWT. Calculations worksheet C-122D attached.**

Approved By Commission:	Conducted By: Bill Trembley, Jr.	Calculated By: Eddie Mahfood	Checked By:
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