

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Dr. File
122 file

Type Test ☒ Initial JUN 1 1977 ☐ Annual ☐ Special						Test Date May 19, 1977	
Company O. C. C. Depco, Inc. ARTESIA, OFFICE				Connection None			
Pool millman atoka millman Atoka - millman				Formation Atoka		Unit	
Completion Date May 19, 1977		Total Depth 11350'		Plug Back TD 11310'		Elevation 3489' KB-12	
Csg. Size 5 1/2"		Wt. 20.0		Set At 11350		Perforations: From 10460' To 10460'	
Thg. Size 2 3/8"		Wt. 4.7		Set At 10425		Perforations: Open ended	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 10425'	
Producing Thru Tubing		Reservoir Temp. °F 170 @ 10464'		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2	
L 10464'		H -		Gg 0.666		% CO ₂ 0.627	
				% N ₂ 1.354		% H ₂ S 0.000	
				Prover		Meter Run 2 X 1.250	
						Taps F	
FARM OR LEASE NAME DHY State B							
COUNTY Eddy							
STATE New Mexico							

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g. DWT	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							1908				65.00
1.	2 4/64	1.250		545	1.69	87	1817			Packer	1.50
2.	2 7/64	1.250		545	4.00	82	1709				1.00
3.	2 9/64	1.250		545	7.84	81	1517				1.00
4.	2 10/64	1.250		545	10.89	81	1345				1.25
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	8.120	30.71	558.2	0.9750	1.225	1.048	312.13
2	8.120	47.24	558.2	0.9795	1.225	1.049	482.82
3	8.120	66.14	558.2	0.9804	1.225	1.049	676.60
4	8.120	77.95	558.2	0.9804	1.225	1.049	797.42
5							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	Dry Gas	Mcf/hbl.
1	0.83	547	1.47	0.911	A.P.I. Gravity of Liquid Hydrocarbons		
2	0.83	542	1.46	0.909	Specific Gravity Separator Gas	0.666	XXXXXXX
3	0.83	541	1.46	0.909	Specific Gravity Flowing Fluid	XXXXX	
4	0.83	541	1.46	0.909	Critical Pressure	671	
5					Critical Temperature	371	

P _c 2695.2		P _c ² 7264.1	
NO.	P _t ²	P _w ²	P _c ² - P _w ²
1	2565.2	6580.3	683.8
2	2435.2	5930.2	1333.9
3	2184.2	4770.7	2493.4
4	1961.2	3846.3	3417.8
5			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.125$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1179$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.478$

Absolute Open Flow 1179 Mcfd @ 15.025		Angle of Slope e62° 8'		Slope, n 0.523	
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Remarks: *** BHP @ (-6975) 10464' used for pressure calculations**

Approved By Commission:	Conducted By: Jarrel Services, Inc	Calculated By: Joe A. Coleman	Checked By: Joe A. Coleman
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