

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 4-15-77		APR 26 1977	
Company Oil Corp. GULF ENERGY MINERALS		Connection AIR		O. C. C. ARTERIA, OFFICE	
Well WILDCAT		Formation Atoka		Unit	
Completion Date 4-14-77		Total Depth 13165 12145		Plug Back TD 11896 11096	
Elevation 3629 Gr.		Form or Lease Name LITTLEFIELD "EM" COM		Well No. 1	
Casing Size 7.00"		Set At 12145		Perforations: From 11102 To 11120	
Casing Size 7.00"		Set At 11050		Perforations: From To	
375 CS Hydril 4.70"		1.995'		Unit Sec. Twp. Pgs. J 20 18 31	
Type Well - Single - Broadhead - G.G. or G.O. Multiple		Packer Set At 11050		County EDDY	
Dual Completion Gas-Gas		Baro. Press. - P _a 13.2		State NEW MEXICO	
Producing Thru Tubing		Reservoir Temp. °F 180 ° 11111		Mech. Annual Temp. °F 60	
L H Gg		% CO ₂ % N ₂ % H ₂ S		Provor	
11111 11111		0.694 0.00 0.02 0.00		Meter Run X	
				Taps FLG.	

FLOW DATA						TUBING DATA		CASING DATA		Direction of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI							3103	70		
1.	4.00		1.50	630	4.00"	102	2680	70		
2.	4.00		1.50	630	9.00"	103	2520	70		
3.	4.00		1.50	645	21.00"	93	2188	70		
4.	4.00		1.50	660	40.00"	73	1693	70		
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super. Comp. Factor, Fpv	Rate of Flow Q, Mscf
1.	10.84	50.723	643.20	0.9619	1.2004	1.0570	671
2.	10.84	76.084	643.20	0.9611	1.2004	1.0580	1007
3.	10.84	117.568	658.20	0.9697	1.2004	1.0620	1575
4.	10.84	164.098	673.20	0.9877	1.2004	1.0760	2269
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	0.96	562	1.45	0.894	14291	57.00	0.694	XXXXXX	669	388
2.	0.96	563	1.45	0.894				XXXXXX	663	451
3.	0.98	553	1.43	0.877						
4.	1.01	533	1.37	0.855						
5.										

NO.	P _t	P _w	P _w ²	P _c ² - P _w ²
1.	3116.2	2696.7	7272	2439
2.		2541.5	6459	3251
3.		2221.2	4934	4777
4.		1747.7	3054	6656

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.45898$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3310$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.45898$

4-28-77

Absolute Open Flow	3310	Mscf @ 15.025	Angle of Slope θ	45	Slope, n	1.00
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Approved by Commission:

Conducted By:

Calculated By:

Checked By: