

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Well file ✓
C-122 file

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 12-20-77		RECEIVED	
Company Gulf Oil Corporation				Connection None		DEC 29 1977			
Pool Angell Ranch manaw irrigated				Formation Morrison		Unit O.C.C.		ARTEZIA, OFFICE	
Completion Date 12-9-77		Total Depth 11000 / 11090		Plug Valve TD 10943 / 10843		Elevation 3363 ft.		Farm or Lease Name Pacheco Federal	
Coq. Size 5 1/2	Wt. 17 & 20	Set At 11000	Perforations: From 10742 To 10830		Well No. # 1				
Tbg. Size 2 3/8	Wt. 4.7	Set At 10695	Perforations: From To		Unit J		Sec. 31	Twp. 19	Rge. 28
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 10695		County Sedg	
Producing Thru Tbg.		Reservoir Temp. °F 181 @ 10695		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State New Mexico	
L 10695	H 10695	G _g .623	% CO ₂ 2.04	% N ₂ 1.12	% H ₂ S	Prover	Meter Run 4"	Taps Flg.	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2729				72 Hr.
1.	4 x .750			535	2	72	2567				1 Hr.
2.	4 x .750			535	20	92	2500				1 Hr.
3.	4 x .750			540	43.5	101	2385				1 Hr.
4.	4 x .750			540	39	103	2165				1 Hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{P_m P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	2.661	70.24	540.2	.9277	1.267	1.043	245
2.	2.661	104.71	543.2	.9706	1.267	1.043	357
3.	2.661	155.12	553.2	.9628	1.267	1.139	576
4.	2.661	221.89	553.2	.9610	1.267	1.139	819
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	.82	523	1.46	.910			.623		671	365
2.	.82	552	1.51	.920						
3.	.82	561	1.54	.926						
4.	.82	563	1.54	.926						
5.										

P _c 2742.2 P _c ² 7519.7						
NO.	P _r ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.735$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.735$
1		2580.7	6560.0	359.6		
2		2514.1	6320.7	1122.0		
3		2400.8	5763.2	1755.3		
4		2184.0	4769.9	2749.8		
5						

Absolute Open Flow 2,240 Mcfd @ 15.025				Angle of Slope θ 45°		Slope, n 1.000	
Remarks:							
Approved By Commission: _____ Conducted By: John Davis Calculated By: Larry Davis Checked By: _____							