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.W MEXICO OIL CONSERVATION CO[...] SION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED
JAN 07 1981
O. C. D.
ARTESIA, OFFICE

Type Test: [X] Initial [ ] Annual [ ] Special

Test Date: 12-23-80

Company	Connection	Unit
MITCHELL ENERGY Corp.	AIR	

Pool	Formation	Unit
WILDCAT morrow	MORROW	B

Completion Date	Total Depth	Plug Back TD	Elevation	Farm or Lease Name
12-14-80	8,150	~~8,087~~ 8097	4,264 KB	STATE 36

Csg. Size	Wt.	d	Set At	Perforations	Well No.
4½	11.6	4.000	8,087	From 7,830 To 7,838	#1

Tbg. Size	Wt.	d	Set At	Perforations	Unit	Sec.	Twp.	Rge.
2 3/8	4.6	1.995	7,750	From PERF. NIPPLE	B	36	19S	21E

Type Well – Single – Bradenhead – G.G. or G.O. Multiple	Packer Set At	County
SINGLE	7,750	EDDY

Producing Thru	Reservoir Temp. °F	Mean Annual Temp. °F	Baro. Press. – P_a	State
TUBING	154 @ 7,730 F	60	13.2	NEW MEXICO

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
7,750	7,750	.6265	.42	.40	Ø		4"	FLANGE

NO.	FLOW DATA: Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					2,251		PACKER		N.A.
1.	4" X 1"	430	2	87	1,971	70			1HR
2.	4" X 1"	430	½	76	1,946	70			1 HR
3.	4" X 1"	440	5	70	1,849	71			1 HR
4.	4" X 1"	450	30	69	1,513	70			1 HR
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	4.758	29.7725	443.2	.9750	1.263	1.035	180.5
2	4.758	14.8862	443.2	.9850	1.263	1.038	91.5
3	4.758	47.6025	453.2	.9905	1.263	1.039	294.4
4	4.758	117.8812	463.2	.9915	1.263	1.041	731.2
5.							

NO.	P_r	Temp. °R	T_r	Z
1	.66	547	1.50	0.934
2.	.66	536	1.47	0.928
3.	.67	530	1.46	0.926
4.	.69	529	1.45	0.922
5				

Gas Liquid Hydrocarbon Ratio ______ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons ______ Deg.
Specific Gravity Separator Gas .6265 XXXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 673 P.S.I.A. 673 P.S.I.A.
Critical Temperature 364 R 364 R

P_c 2,833.2 P_c^2 8,027.0

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	3937.0	2,498.2	6241.0	1786.0
2	3838.5	2,439.2	5949.7	2077.3
3	3467.8	2,350.2	5523.4	2503.9
4	2329.3	1,937.2	3752.7	4274.3
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2}$ = 1.8780 (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ = 1.78

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ = 1,301.5

Absolute Open Flow 1,301.5 Mcfd @ 15.025 Angle of Slope θ 46 Slope, n 1.000

Remarks: CACULATED FROM KNOWN BOTTOMHOLE PRESSURES. MEASURED WITH AMERADA PRESSURE ELEMENT RPG3 #44631, 0-4,000 LB. RANGE

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Don Bennett	Don Bennett	[signature]