

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

c/sf
File
Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 10-22-82		NOV 8 1982	
Company Amoco Production Company ✓				Connection Atmosphere		O. C. D.	
Pool Undesignated				Formation Wolfcamp		Unit ARTESIA, OFFICE	
Completion Date 10-6-82 11-3-82		Total Depth 8744.		Plug Back TD 7615.		Elevation 3737.	
Csq. Size 5.500		Wt. 17.0		Set At 8744.		Perforations: From 6338. To 6346.	
Thq. Size 2.375		Wt. 4.7		Set At 6190		Perforations: From 0. To 0.	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 6104.		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 105. @ 6342		Mean Annual Temp. °F 60.0		Baro. Press. - P _a 13.2	
L 6104.		H 6104.		G _q 0.644		% CO ₂ 0.25	
				% N ₂ 2.44		% H ₂ S 0.	
				Prover 2.0		Meter Run 0.	
						Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							1949.	47.			137.0
1.	2.00 x 0.063			1875.	1879.0	45.	1879.	45.	0.	0.	1.0
2.	2.00 x 0.125			1600.	1602.0	47.	1602.	47.	0.	0.	1.0
3.	2.00 x 0.188			1185.	1188.0	46.	1188.	46.	0.	0.	1.0
4.	2.00 x 0.250			1052.	1055.0	44.	1055.	44.	0.	0.	0.25
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	0.06	1883.59	1888.2	1.0147	1.2461	1.1954	182.
2.	0.26	1607.59	1613.2	1.0127	1.2461	1.1750	632.
3.	0.61	1193.09	1198.2	1.0137	1.2461	1.1347	1042.
4.	1.08	1060.09	1065.2	1.0157	1.2461	1.1208	1639.
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	2.83	505.	1.38	0.700	0.	
2.	2.42	507.	1.39	0.724	A.P.I. Gravity of Liquid Hydrocarbons 0.	
3.	1.80	506.	1.39	0.777	Specific Gravity Separator Gas 0.644	XXXXXXX
4.	1.60	504.	1.38	0.796	Specific Gravity Flowing Fluid XXXXX	0.644
5.					Critical Pressure 667. P.S.I.A.	667. P.S.I.A.
					Critical Temperature 365. R	365. R

P _c 1973.1 P _c ² 3893.				
NO.	P _i ²	P _w	P _w ²	P _i ² - P _w ²
1.	3580.	1904.	3627.	266.
2.	2609.	1626.	2643.	1250.
3.	1443.	1214.	1474.	2419.
4.	1141.	1094.	1196.	2697.
5.				

(1) $\frac{P_c^2}{P_i^2 - P_w^2} = 1.4436$

AOF = Q $\left[\frac{P_c^2}{P_i^2 - P_w^2} \right]^n = 1517.0$

(2) $\left[\frac{P_c^2}{P_i^2 - P_w^2} \right]^n = 1.4563$

Post FD 2
11-19-82
Group 4 BK

Absolute Open Flow 1517.0 Mcfd @ 15.025	Angle of Slope @ 38.3	Slope, n .79
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Remarks: Fourth data point flowed only 15 minutes due to water production.

Approved By Commission:	Conducted By: John West Engr.	Calculated By: Richard Roeth	Checked By: Steven F. Leskier
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