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ARTESIA, OFFICE

NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 6-1-65

Type Test: [x] Initial [ ] Annual [ ] Special				Test Date: 11/3/83	~~1980 FNL~~
Company: Mitchell Energy Corporation ✓			Connection: Transwestern Pipeline Company		~~1739 FWL~~
Pool: Turkey Track – ~~Wildcat~~			Formation: Morrow		Unit: ~~F~~
Completion Date: ~~7/27/81~~ 9-28-83	Total Depth: 11,461'		Plug Back TD: 11,432'	Elevation: 3398 KB	Farm or Lease Name: Flag "TD" State Com
Csg. Size: 5 1/2"	Wt.: 17/20	d: 4.778	Set At: 11461	Perforations: From 10981 To 11078	Well No.: 1
Tbg. Size: 2 7/8"	Wt.: 6.5	d: 2.441	Set At: 10,800	Perforations: From open To ended	Unit: F Sec.: 18 Twp.: 19S Rge.: 29E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single			Packer Set At: 10,800		County: Eddy
Producing Thru: Tubing	Reservoir Temp. °F: 168 @ 11030		Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2	State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
11030	11030	.640	.730	.675	0	-	2"	Flange

NO.	FLOW DATA: Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI						2755	75	pkr		95 hrs
1.	2"	1"	380	18"	69	2350	69			2
2.	2"	1"	380	38"	69	2150	69			2
3.	2"	1"	400	60"	69	1900	69			2
4.	2"	1"	400	90"	69	1600	69			2
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	4.946	84.13	393.2	.9915	1.199	1.047	518
2.	4.946	122.24	393.2	.9915	1.199	1.047	753
3.	4.946	157.45	413.2	.9915	1.199	1.049	971
4.	4.946	192.84	413.2	.9915	1.199	1.049	1189
5.							

NO.	P_t	Temp. °R	T_r	Z
1.	.589	529	1.349	.913
2.	.589	529	1.349	.913
3.	.619	529	1.349	.909
4.	.619	529	1.349	.909
5.				

Gas Liquid Hydrocarbon Ratio 52.174 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons 57.0 Deg.
Specific Gravity Separator Gas .640 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX .696
Critical Pressure 670 P.S.I.A. 668 P.S.I.A.
Critical Temperature 372 R 392 R

P_c 2768.2 P_c^2 7662.9

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	5584.7	2364.3	5589.9	2073
2	4679.4	2165.7	4690.2	2972.7
3	3660.3	1917.8	3678.0	3984.9
4	2602.4	1621.4	2628.9	5034
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.522$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.426$

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1696$

Post ID-2
12-16-83
Comp + BK

Absolute Open Flow 1696 Mcfd @ 15.025 Angle of Slope @ 49.8° Slope, n .845

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Darryl White	Dan Tuffly	