

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS RECEIVED BY

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 10/1/85		JUL - 8 1986 O. C. D. ARTESIA OFFICE	
Company Exxon Corp. ✓				Connection None					
Pool Antelope Sink - Strawn <i>Wood at Strawn</i>				Formation <i>Strawn Atoka</i>		Unit H			
Completion Date 9/16/85		Total Depth 8616		Plug Back TD 7850		Elevation		Farm or Lease Name Panos Federal Com.	
Csg. Size 5 1/2	Wt. 15#	d 4.950	Set At 8616	Perforations: From 7564 To 7631		Well No. 1			
Tbg. Size 2 7/8	Wt. 6.5	d 2.441	Set At 7520	Perforations: From Open To End		Unit H	Sec. 1	Twp. 19S	Rye. 23E
Type Well - Single - Brdhead - G.G. or G.O. Multiple Single						Packer Set At 7520		County Eddy	
Producing Thru Tbg.		Reservoir Temp. °F 149 @ 7520		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State New Mexico	
L 7520	H 7520	Gg .714	% CO ₂ 10.379	% N ₂ .592	% H ₂ S	Prover	Meter Run 4.026	Taps Flg.	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI							1895			
1.	4.026 X .750			300	9	73	1757			
2.	4.026 X .750			300	22	74	1594			
3.	4.026 X .750			300	35	70	1375			
4.	4.026 X .750			310	59	75	1095			
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	2.661	53.09	313.2	.9877	1.183	1.029	170
2	2.661	83.01	313.2	.9868	1.183	1.029	265
3	2.661	104.70	313.2	.9905	1.183	1.029	336
4	2.661	138.09	323.2	.9859	1.183	1.029	441
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Dry	Mcf/bbl.
1.	.44	533	1.41	.945	A.P.I. Gravity of Liquid Hydrocarbons _____	Deq.
2.	.44	534	1.41	.945	Specific Gravity Separator Gas .714	XXXXXXXXXX
3.	.44	530	1.40	.944	Specific Gravity Flowing Fluid XXXXX	
4.	.45	535	1.42	.945	Critical Pressure 712 P.S.I.A.	P.S.I.A.
5.					Critical Temperature 378 °R	°R

NO.	P _i ²	P _w ²	P _w ²	P _c ² - P _w ²
1		1770.3	3133.8	507.4
2		1607.4	2583.7	1057.5
3		1388.6	1928.1	1713.1
4		1109.0	1229.9	2411.3
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.510$

AOF = 0 $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = .566$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.284$

Absolute Open Flow 566 Mcfd @ 15.025	Angle of Slope 58.75	Slope, n .607
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Remarks: Well Made No Fluid During Test

Approved By Division	Conducted By: Duke Services, Inc.	Calculated By: R. Reston	Checked By:
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