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appropriate district office
See Rule 401 & Rule 1122

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

OCT 11 '94

O. C. D.

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator MARALO, INC.				Lease or Unit Name STATE "11" COM			
Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 10-4-94		Well No. 1	
Completion Date 08-17-94		Total Depth 11228		Plug Back TD 11228		Elevation 3419' GR	
Unit Ltr. Sec. TWP. Rge. 1 11-19S-28E		County EDDY		Pool Turkey Track		UNDERSIG- MORROW	
Csg. Size 5 1/2	Wt. 17#	d	Set At 11007	Perforations: From: 11066 To: 11074		Formation MORROW	
Tbg. Size 2 7/8	Wt. 11045	d	Set At 11045	Perforations: From: To:		Connection Pipeline	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple single				Packer Set At 11007		Meter Run 4.026	
Producing Thru tbq.		Reservoir Temp. °F 60°		Mean Annual Temp. °F 60°		Baro. Press - P. 13.2	
L *11037	H *11037	Gg .628	% CO ₂ .70	% N ₂ .28	% H ₂ S	Prover	Taps alg.

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	Orifice X Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI						2890				
1.	4.026	X 1.500	200	5	79	2665		pk		1 hr.
2.	4.026	X 1.500	275	14.5	70	2405		"		1 hr.
3.	4.026	X 1.500	300	30	62	2080		"		1 hr.
4.	4.026	X 1.500	310	56	84	1685		"		1 hr.
5.										

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	10.84	32.65	213.2	.9822	1.262	1.019	447
2.	10.84	64.64	288.2	.9905	1.262	1.025	898
3.	10.84	96.93	313.2	.9981	1.262	1.030	1,363
4.	10.84	134.53	323.2	.9777	1.262	1.025	1,844
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio DRY GAS Mcf/bbl.		
1.	.31	539	1.47	.964	A.P. I. Gravity of Liquid Hydrocarbons DRY Deg.		
2.	.42	530	1.45	.951	Specific Gravity Separator Gas .628 XXXXXXXXXX		
3.	.46	522	1.43	.942	Specific Gravity Flowing Fluid XXXXXX		
4.	.48	544	1.49	.951	Critical Pressure 671 P.S.I.A. P.S.I.A.		
5.					Critical Temperature 365 R R		

P _c 2987.8		P _c ² 8926.9			1) $\frac{P_c^2}{P_c^2 - P_w^2} = \underline{1.542}$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{1.525}$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{2.812}$			
1.		2767.6	7659.6	1267.3				
2.		2488.8	6194.1	2732.8				
3.		2169.4	4706.3	4220.6				
4.		1771.3	3137.5	5789.4				
5.								

Absolute Open Flow	2,812	Mcf @ 15.025	Angle of Slope Θ 46	Slope, n .97367
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Remarks: **NO FLUID PRODUCED DURING TEST**
* = BHP INSTRUMENT SET @ THIS DEPTH

Approved By Division	Conducted By: PRO WELL TESTER	Calculated By: BM	Checked By: BM
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