Submit in duplicate to appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Depar. :nt

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

RECEIVED
JUN 12 1996
INTERCOAST OIL and GAS

dsf

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator: Medallion Production Company					Lease or Unit Name: Tweedy "9"		
Type Test: [X] Initial [ ] Annual [ ] Special					Test Date: 6-10-96	Well No.: 1	
Completion Date: 3-21-96	Total Depth: 9625'		Plug Back TD: 9578'		Elevation: GL=3464'	Unit Ltr. - Sec. - TWP - Rge.: J 9- 20S-25E	
Csg. Size: 4½"	Wt.: 11.6	d: N-80	Set At: 9625'	Perforations: From: 9496' To: 9504'		County: Eddy	
Tbg. Size: 2-3/8"	Wt.: 4.7	d: N-80	Set At: 9400'	Perforations: From: To:		Pool: Cemetary ~~Undes~~, Morrow	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple: Single			Packer Set At: 9400'			Formation: Morrow	
Producing Thru: Tubing	Reservoir Temp. °F: 151°	Mean Annual Temp. °F		Baro. Press - P_a		Connection: El Paso NG	
L: 9400	H: 9400	Gg: 0.593	% CO_2: 0.981	% N_2: 0.232	% H_2S: 0	Meter Run	Taps

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FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI							1327		Pkr		24 Hrs.
1.	4	X	2.000				1265		"		1 Hr.
2.	4	X	2.000				1167		"		1 Hr.
3.	4	X	2.000				812		"		1 Hr.
4.	4	X	2.000				472		"		1 Hr.
5.											

RATE OF FLOW CALCULATIONS

NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F pv.	Rate of Flow Q, Mcfd
1.							469
2.		FLOW MEASURED BY TOTAL FLOW METER					963
3.							2,080
4.							2,503
5.							

NO.	P_r	Temp. °R	T_r	Z
1.				
2.				
3.		NOT NEEDED		
4.				
5.				

Gas Liquid Hydrocarbon Ratio: Dry Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: Dry Gas Deg.
Specific Gravity Separator Gas: .593 XXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 672 P.S.I.A. P.S.I.A.
Critical Temperature: 354 R R

P_c 1340.2 P_c^2 1796.1

NO.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1.		1280.2	1639.9	156.2
2.		1191.2	1419.0	377.2
3.		898.2	807.3	988.8
4.		652.3	425.5	1370.7
5.				

1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.816$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.593$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3.313$

Absolute Open Flow: 3,313 Mcfd @ 15.025 | Angle of Slope θ: 51.98 | Slope, n: 0.78

Remarks: NO FLUID PRODUCED

Approved By Division	Conducted By:	Calculated By:	Checked By:
	WEST-TEST, INC.	B.M.	B.M.

COMPANY :	MEDALLION PROD. CO	LEASE :	ED 9	WELL NO. :	1				
UNIT :	J	SECTION :	9	TOWNSHIP :	20				
L :	9400	H :	9400	L/H :	1	G/GMIX :	0.593		
%CO2 :	0.981	%N2 :	0.232	H2S :		DATE :	6 10 96		
d :	1.995	Fr :	0.018231	GH :	5574.2	RANGE :	25		

VOL 1 :	469	PSIA 1 :	1278.2			RESV.TEMP	168.0
VOL 2 :	963	PSIA 2 :	1180.2				
VOL 3 :	2080	PSIA 3 :	825.2			SHUT-IN PR=	1340.2
VOL 4 :	2503	PSIA 4 :	485.2				
				PCR :	672		
				TCR :	354		

LINE	RATE 1		RATE 2		RATE 3		RATE 4	
	1ST	2ND	1ST	2ND	1ST	2ND	1ST	2ND
1 QM	0.469	0.469	0.963	0.963	2.080	2.080	2.503	2.503
2 TW	534	534	534	534	534	534	534	534
3 Ts	628.0	628.0	628.0	628.0	628.0	628.0	628.0	628.0
4 T	581.0	581.0	581.0	581.0	581.0	581.0	581.0	581.0
PR (est)	1.90		1.76		1.23		0.72	
5 Z(est)	0.857	0.848	0.864	0.854	0.893	0.881	0.925	0.910
6 TZ	498.1	492.5	502.1	496.3	518.8	511.9	537.4	528.6
7 GH/TZ	11.192	11.318	11.102	11.231	10.745	10.889	10.373	10.545
8 eS	1.521	1.529	1.516	1.524	1.496	1.504	1.475	1.485
9 1-e-S	0.343	0.346	0.341	0.344	0.332	0.335	0.322	0.327
10 Pt	1278.2	1278.2	1180.2	1180.2	825.2	825.2	485.2	485.2
11 Pt2 /1000	1633.8	1633.8	1392.9	1392.9	681.0	681.0	235.4	235.4
12 Fr	0.018231	0.018231	0.018231	0.018231	0.018231	0.018231	0.018231	0.0182311
13 Fc=FrTZ	9.080	8.979	9.153	9.048	9.458	9.333	9.797	9.637
14 FcQm	4.26	4.21	8.81	8.71	19.67	19.41	24.52	24.12
15 L/H(FcQm)	18.1	17.7	77.7	75.9	387.0	376.8	601.3	581.9
16 Fw	6.216196	6.133313	26.45952	26.09759	128.3493	126.3342	193.7823	190.05240
17 Pw2	1640.0	1639.9	1419.3	1419.0	809.3	807.3	429.2	425.5
18 Ps2	2495.3	2507.0	2152.3	2162.1	1210.9	1214.4	633.3	631.8
19 Ps	1579.6	1583.3	1467.1	1470.4	1100.4	1102.0	795.8	794.9
20 P	1428.9	1430.8	1323.6	1325.3	962.8	963.6	640.5	640.0
21 Pr	2.13	2.13	1.97	1.97	1.43	1.43	0.95	0.95
22 Tr	1.64	1.64	1.64	1.64	1.64	1.64	1.64	1.64
23 Z	0.848	0.848	0.854	0.854	0.881	0.881	0.910	0.910

Pc =	1340.2	Pc2 =	1796.1
Pt2 =	1633.8	Pw =	1280.6
	1392.9		1191.2
	681.0		898.5
	235.4		652.3
Pc2-Pw2=	156.2	Pw2 =	1639.9
	377.2		1419.0
	988.8		807.3
	1370.7		425.5
n =	0.780		
Pc2/(Pc2-Pw2) =	11.498		
	4.762		
	1.816		
	1.310		
[Pc2/Pc2-Pw2]n =	6.719		
	3.378		
	1.593		
	1.235		
AOF= Q	3.151		
	3.253		
	3.313		
	3.091		

FORM C122-D