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appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

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SEP 06 1996

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator OXY USA INC				Lease or Unit Name OXY USA INC			
Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 8-27-1996		Well No. DIST. 2	
Completion Date 7-27-1996		Total Depth 11286.		Plug Back TD 10090.		Elevation 3306.	
Csg. Size 5.500		Wt. 4.9		Set At Perforations: From: 8952. To: 9094.		Unit Ltr. - Sec. - TWP - Rge. P 33 19S 28E	
Tbg. Size 2.375		Wt. 2.0		Set At 8852		Perforations: From: 0. To: 0.	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At 8852.		Formation WOLFCAMP	
Producing Thru TUBING		Reservoir Temp. °F 60		Mean Annual Temp. °F 60		Baro, Press - P _a 13.2	
Connection NGPL PIPELINE		Meter Run 3.1		Taps FLANGE			
L 9023		H 9023		Gg .685		% CO ₂ .27	
				% N ₂ 1.21		% H ₂ S .00	
				Prover 0			

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI									4215.	149.	92.2
1.	3.07	X	1.500	535.	8.2	96.	0.	0.	4214.	149.	1.0
2.	3.07	X	1.500	542.	23.8	86.	0.	0.	4164.	149.	1.0
3.	3.07	X	1.500	562.	52.3	68.	0.	0.	4097.	149.	1.0
4.	3.07	X	1.500	565.	101.5	57.	0.	0.	4017.	149.	1.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	11.13	67.01	548.2	.9671	1.2082	1.0485	913.
2.	11.13	115.02	555.2	.9759	1.2082	1.0527	1589.
3.	11.13	173.49	575.2	.9924	1.2082	1.0624	2459.
4.	11.13	242.25	578.2	1.0029	1.2082	1.0682	3489.
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P. L. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature	Mcf/bbl.	Deg.
1.	.82	556.	1.46	.910	12.6	56.0	.685	XXXXXX	667.	381.	881	881
2.	.83	546.	1.43	.902				XXXXXX				
3.	.86	528.	1.38	.886								
4.	.87	517.	1.36	.876								
5.												

P _c 2968.5	P _c 8812.											
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	1) $\frac{P_c^2}{P_c^2 - P_w^2} = 8.8661$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.9776$						
1.	17869.	2968.	8807.	5.								
2.	17449.	2924.	8549.	263.								
3.	16894.	2866.	8211.	601.								
4.	16243.	2796.	7818.	994.								
5.												

Absolute Open Flow	12367.	Mcf @ 15.025	Angle of Slope θ	59.5	Slope, n	.589
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Remarks: UNABLE TO ACHIEVE 25% DRAWDOWN DUE TO FLOW LINE SIZE/LIMITATIONS

Approved By Division	Conducted By: Chuck Avery	Calculated By: M.R.	Checked By:
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