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Submit in duplicate to
appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator OXY USA				Lease or Unit Name OXY CHECKER STATE			
Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 23-JUL-1997		Well No. 1	
Completion Date		Total Depth 11,470		Plug Back ID 10,515		Elevation	
Csg. Size 4.5		Wt. d 11.6		Set At 11,470		Unit Ltr. - Sec. - TWP - Rge. L 8-19-29	
Tbg. Size 2.375		Wt. d 4.7		Set At 9,815		Country EDDY	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE GAS WELL				Packer Set At 9813.4		Pool TURKEY TRACK CANYON	
Producing Thru 9949		Reservoir Temp. °F 150 @ 9949		Mean Annual Temp. °F 50		Formation CANYON	
Baro. Press - P _a 13.2		Connection CONOCO		Meter Run 4.016		Taps FLANGE	
G _g 0.736		% CO ₂ 0.64		% N ₂ 1.47		% H ₂ S 0	
Prover		Prover		Prover		Prover	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI									1784	160	01.7
1.	4.02	X	1.375	170	65.4	70			1756	160	1.0
2.	4.07	X	1.375	178	90.8	55			1657	160	1.0
3.	4.07	X	2.625	187	8.1	59			1580	160	1.0
4.	4.07	X	2.625	195	13.2	65			1408	160	1.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.		109.46	183.2	0.9907	1.1656	1.0211	1352
2.		131.76	191.2	1.0040	1.1656	1.0241	1511
3.		40.22	199.7	1.0007	1.1656	1.0247	1919
4.		52.52	209.0	0.9952	1.1656	1.0250	2415
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	0.28	530	1.34	0.959	A.P. I Gravity of Liquid Hydrocarbons 55.0	Deg.
2.	0.29	516	1.30	0.953	Specific Gravity Separator Gas 0.736	XXXXXXXXXX
3.	0.30	519	1.31	0.952	Specific Gravity Flowing Fluid	XXXXXX
4.	0.31	525	1.33	0.952	Critical Pressure 666	P.S.I.A. 553 P.S.I.A.
5.					Critical Temperature 396	R 413 R

P _c 1253.7	P _c ² 1572									
NO.	P _c ²	P _w	P _w ²	P _c ² - P _w ²	1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.8725$			(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.5948$		
1.	3131	1236	1527	44	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4093$					
2.	2824	1179	1390	182						
3.	2537	1123	1250	311						
4.	2021	1012	1025	547						
5.										

Absolute Open Flow **4093** Mcfd @ 15.025 Angle of Slope θ **63.4** Slope, n **0.500**

Remarks: **BASED ON BOTTOM HOLE PRESSURE**

Approved By Division _____ Conducted By: *Kerry Davis* Calculated By: *Robert Beckham* Checked By: _____