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appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources

Form C-122
Revised October, 1999

Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator Fasken Oil and Ranch, Ltd.					Lease or Unit Name Howell "29" Com				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 8-6-01		Well No. 2		
Completion Date 7-21-01		Total Depth 9,700'		Plug Back TD 9,658'		Elevation 3553'		Unit Ltr. - Sec. - TWP - Rge. D 29 20S 25E	
Csg. Size 4-1/2"	Wt. 11.6	d 4.000	Set At 9,700'	Perforations: From: 9496' To: 9556'				County Eddy	
Tbg. Size 2-7/8"	Wt. 6.5	d 2.441	Set At 9,481'	Perforations: From: To:				Pool Cemetery	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 9,470'		Formation Morrow			
Producing Thru Tubing		Reservoir Temp. °F 168		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		Connection El Paso Field Services	
L 9481	H 9481	Gg 0.625	%CO ₂ 0.83	%N ₂ 0.20	%H ₂ S 0.00	Prover Orifice	Meter Run 3"	Taps Flange	

FLOW DATA					TUBING DATA		CASING DATA			Duration Of Flow
No.	Prover Line Size	Orifice X Size	Press. p.s.i.g.	Diff. H _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI						2362	75	0	75	--
1.	3.068" x 1.25"		60	27.2	75	60	75	0	75	24 hr
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS							
No.	COEFFICIENT (24 HOUR)	h _w P _m	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	7.577	44.63	73.2	0.9859	1.265	1.010	426
2.							
3.							
4.							
5.							

No.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	0.108	535	1.466	0.980	A. P. I. Gravity of Liquid Hydrocarbons	Deg.
2.					Specific Gravity Separator Gas 0.625	XXXXXXXXXX
3.					Specific Gravity Flowing Fluid 0.625	XXXXXX
4.					Critical Pressure 674	P.S.I.A. P.S.I.A.
5.					Critical Temperature 365	R. R.

No.	P _c	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{5641.6}{5634.0}$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0013$
1.	5.4	87.0	7.6	5634.0		
2.						
3.						
4.						
5.						

AO = **427** Mcfd @ 15.025

Angle of Slope θ: **45**

Slope, n: **1.0**

Remarks:

Approved By Division	Conducted By: Fasken Oil and Ranch, Ltd.	Calculated By: Carl Brown	Checked By:
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