

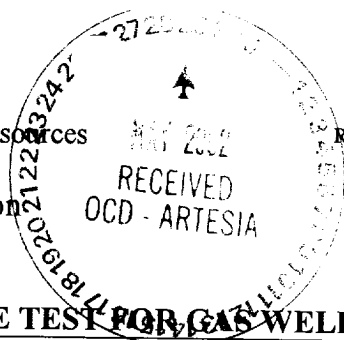
Submit in duplicate to
appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources

Form C-122

Revised October, 1999

Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505



MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator Fasken Oil and Ranch, Ltd.					Lease or Unit Name Cameron "31" Federal				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 5-2-02		Well No. 2		
Completion Date 9-1-02		Total Depth 9804'		Plug Back TD 9736'		Elevation 3666' GR		Unit Ltr. - Sec. - TWP - Rge. H 31 20S 25E	
Csg. Size 4-1/2"	Wt. 11.6	d 4.000	Set At 9804'	Perforations: From: 9602' To: 9626'				County Eddy	
Tbg. Size 2-3/8"	Wt. 4.7	d 1.995	Set At 9356'	Perforations: From: To:				Pool Cemetery	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single					Packer Set At 9354'		Formation Morrow		
Producing Thru Tubing		Reservoir Temp. °F 168		Mean Annual Temp. °F 60		Baro. Press - P. 13.2		Connection Fasken - Transporter	
L 9356'	H 9356'	Gg 0.591	%CO ₂ 0.41	%N ₂ 0.87	%H ₂ S 0.00	Prover	Orifice 3"	Meter Run Flange	Taps

FLOW DATA					TUBING DATA		CASING DATA		Duration Of Flow
No.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI						3165	80	0	80
1.	3.068" x 1.25"		55	15.8	80	55	80	0	80
2.									
3.									
4.									
5.									

RATE OF FLOW CALCULATIONS							
No.	COEFFICIENT (24 HOUR)	h _w P _m	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	7.577	32.88	68.2	0.9813	1.265	1.01	312
2.							
3.							
4.							
5.							

No.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	0.10	540	1.479	0.98	A. P. I. Gravity of Liquid Hydrocarbons	Deg.
2.					Specific Gravity Separator Gas 0.591	XXXXXXXXXX
3.					Specific Gravity Flowing Fluid 0.591	XXXXXX
4.					Critical Pressure 673	P.S.I.A.
5.					Critical Temperature 351	R.

P _c 3178	P _c ² 10099.7
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No.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{10099.7}{10091.8}$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0007$
1.	4.7	88.8	7.5	10091.8		
2.						
3.						
4.						
5.						

AOF = Q (312)

$\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 312$

AOF = Q (312)

$\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 312$

Absolute Open Flow 312	Mcf/d @ 15.025	Angle of Slope θ: 45	Slope, n: 1.00
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Remarks:
An approximation of AOF was made with unit slope through the maximum rate.

Approved By Division	Conducted By: Fasken Oil and Ranch, Ltd.	Calculated By: Carl Brown	Checked By:
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