

NE MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

copy to J.F.

RECEIVED

Type Test ☐ Initial ☐ Annual ☒ Special		Test Date 6-8-66		JUL 5 1966							
Company Standard Oil Company of Texas ; Marathon Oil Company			Connection Cisco Canyon								
Well Indian Basin (Upper Basin)			Formation Cisco Canyon		Unit Eagle Flats						
Completion Date 6-27-65		Total Depth 7690	Plug Back TD 7560	Elevation 4021 Gr	Farm or Lease Name Eagle Flats Unit						
Case Size 5 1/2	Wt. 25.5	Set in 4 980	7690	Perforations: From 7143 To 7306	Well No. 4						
Tool Size 2	Wt. 7	Set in 1.995	7074	Perforations: From None To	Unit Sec. Twp. Rge. F 10 22S 23E						
Type No. - Single - Annular - C.G. or C.O. Multiple Single			Packer Set At 7060		County Eddy						
Producing Time Following		Reservoir Temp. °F 132 @ 7074	Mean Annual Temp. °F 60	Baro. Press. - P _a 13.2	State New Mexico						
L 7074	R 7074	G _v .626	% CO ₂ .54	% N ₂ .90	% H ₂ S .33						
Prover			Meter Run 3.068	Taps Flange							
FLOW DATA											
NO.	Packer Size	X	Casing Size	Press. Producing	Diff. hwy	Temp. °F	Press. Producing	Temp. °F	Press. Producing	Temp. °F	Duration of Flow
1	3.068	1.625	7.0	3.4	1	73	2875	73	Packer		36 Hrs.
2	3.068	1.625	7.0	5.5	2	74	2875	74			75 Min.
3	3.068	1.625	7.0	7.2	3	75	2875	75			105 Min.
4	3.068	1.625	7.0	8.9	4	72	2877	74			135 Min.
5	3.068	1.625	7.0								90 Min.
RATE OF FLOW CALCULATIONS											
NO.	Coeff. m _g (G. Hour)	$\sqrt{P_a - P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super. Compress. Factor, F _{sp}	Rate of Flow Q, Mcfd				
1	59.31	24.02	1065.0	.9397	1.234	1.065	1,918				
2	59.31	40.15	1065.8	.9304	1.234	1.051	3,155				
3	59.31	52.56	1065.8	.9359	1.234	1.055	4,208				
4	59.31	64.97	1065.0	.9367	1.234	1.055	5,231				
NO.	T ₁	Temp. °F	T ₂	Z	Gas Liquid Hydrocarbon Ratio 142.4 Mcf/bbl.						
1	1.53	551	1.51	.851	A.P.I. Gravity of Liquid Hydrocarbons 57.5 Deg.						
2	1.53	547	1.51	.853	Specific Gravity Separator Gas .626		XXXXXXXXXX				
3	1.53	545	1.51	.849	Specific Gravity Flowing Fluid XXXXX		.646				
4	1.53	542	1.48	.845	Critical Pressure From Analysis 674.7 P.S.I.A.		673 P.S.I.A.				
					Critical Temperature From Analysis 358.5 °R		360 °R				
$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{37.05}{1065^2 - 1065^2} = 37.05$					$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{12.49}{1065^2 - 1065^2}$						
$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 65.340$											
Actual Open Flow 65.340 Mcfd @ 13.025					Angle of Slope @		Slope, n .699				
Remarks: 200' x 200' Section # 65 4.372 Sec. # 1004 x 3000' x 1000' x 1000' x 1000'											
Approved By Commission:		Conducted By: D. F. Jones		Calculated By: R. W. Harrington		Checked By:					