

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELLS

Form C-122
Revised 9-1-65

AUG 7 1967

Type Test ☐ Initial ☐ Annual ☒ Special		Test Date 7-25-67		O.C.S. ARTESIA, OFFICE	
Company PENNZOIL COMPANY		Connection DELHI GAS PIPELINE CORP.		Unit 320 ACRES	
Pool UNDESIGNATED		Formation STRAWN		Farm or Lease Name HUDSON FEDERAL	
Completion Date 9-25-66		Total Depth 11653'		Plug back TD 11170'	
Elevation 3429' GL		Well No. 1		County EDDY	
Csg. Size 5 1/2"		Wt. 17.0		d 4.892	
Set At 11475		Perforations From 11000' To 11102'		Unit Sec. Twp. Rge. C 4 21s 29E	
Tng. Size 2 3/8"		Wt. 4.7		d 1.995	
Set At 10976		Perforations OPEN ENDED		State NEW MEXICO	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packoff Set At 10970'	
Producing Thru TUBING		Reservoir Temp. *F 176 @ 10900		Mean Annual Temp. *F -	
L 10976		H -		Gg 0.669	
% CO ₂ 0.17		% N ₂ 0.06		% H ₂ S 0.00	
Prover -		Meter Run -		Taps FLANGE	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. *F	Press. p.s.i.g.	Temp. *F	Press. p.s.i.g.	Temp. *F	
SI	4		2.750				4120				144 HRS
1.	4		2.750	325	16"	78	2775	78	PKR	-	2.0
2.	4		2.750	325	14"	80	2822	80	-	-	1.25
3.	4		2.750	320	11"	80	3177	80	-	-	1.25
4.	4		2.750	310	7"	80	2510	80	-	-	1.25
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor F_t	Gravity Factor F_g	Super Compress. Factor, F_{pv}	Rate of Flow Q, Mcld
1	41.10	73.56	338	1.035	1.224	1.139	4278.1 382%
2	41.10	68.82	338	1.035	1.224	1.139	4002.4 315%
3	41.10	60.55	333	1.035	1.224	1.039	3206.0
4	41.10	50.84	323	1.035	1.224	1.038	2694.5
5.							

NO.	P_f	Temp. *R	T_f	Z	Gas Liquid Hydrocarbon Ratio	Mcld/bbl.
1	0.50	505	1.35	0.926	14301	
2	0.50	505	1.35	0.926	56.7	
3	0.50	507	1.36	0.927	0.668	XXXXXXX
4	0.48	505	1.35	0.920	XXXXX	-
5.						

NO.	P_c^2	P_w^2	R_w^2	$P_c^2 - R_w^2$	(1) $\frac{P_c^2}{P_c^2 - R_w^2} = \frac{P_c^2}{R_c^2 - R_w^2}$	(2) $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = \frac{P_c^2}{R_c^2 - R_w^2}$
1	-	4262.2	18166.9	5092.8		
2	-	4413.2	19476.3	3772.8		
3	-	1758.2	22640.5	10608.6		
4	-	5111.2	26124.4	7124.4		
5						

Absolute Open Flow		8050	5840	Volume 15.035	Angle of Slope θ	51°	Slope, n	0.803
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Remarks: * BHP @ (-7671') 11100' USED FOR PRESSURE CALCULATIONS	
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Approved By Commission	Conducted By: COLEMAN	Calculated By:	Checked By:
P. J. [Signature]	PETRO. ENG. CO.	JOE A. COLEMAN	JOE A. COLEMAN