

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR S WELL

Form C-122

4/57

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 10/20/1999	
Company YATES PETROLEUM CORPORATION				Connection NAVAJO REFINING COMPANY			
Pool INDIAN BASIN				Formation UPPER PENN ASSOC.		Unit	
Completion Date 9/20/1999		Total Depth 10200		Plug Back TD 10158		Elevation 4172	
Farm or Lease Name HICKORY ALV FEDERAL							
Csg. Size 6.625	Wt. 24.000	d 5.921	Set At 7913	Perforations: From 7970 To 7992		Well No. 2	
Tbg. Size 2.875	Wt. 6.500	d 2.441	Set At 7913	Perforations: From 7970 To 7992		Unit D	Sec. 18
Type Well Single						Packer Set At 7913	Twp. 22S
Producing Thru Tubing						Baro. Press. - Pa 13.2	Rge. 24E
Resv. Temp. °F 130 @ 7900						State NEW MEXICO	
Mean Temp. °F 62		Gg 0.654		%CO ₂ 0.619	%N ₂ 0.863	%H ₂ S 0.000	Prover 0.000
L 10200	H 10200	Meter Run 3.000		Taps Flange			

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
Sl.	0.000	x	0.000	0	0.0	0	190	0			0
1.	3.068	x	1.200	160	22.0	60	170	60			24
2.	3.068	x	1.200	160	27.0	60	167	60			24
3.	3.068	x	1.200	160	33.0	60	163	60			24
4.	3.068	x	1.200	160	38.0	60	160	60			24
5.		x									

NO.	Coefficient (24 Hour)	$\sqrt{hwPm}$	Pressure Pm	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor Fpv	Rate of Flow Q, Mcfd
1.	6.095	61.7	173.2	1.0000	1.237	1.017	473
2.	6.095	68.4	173.2	1.0000	1.237	1.017	524
3.	6.095	75.6	173.2	1.0000	1.237	1.017	579
4.	6.095	81.1	173.2	1.0000	1.237	1.017	622
5.							

NO.	Pr	Temp °R	Tr	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature	Mcf/bbl. Deg.
1.	0.26	520	1.40	0.967	0	0.000	0.654	XXXXXXX	671	370	0.654
2.	0.26	520	1.40	0.967							
3.	0.26	520	1.40	0.967							
4.	0.26	520	1.40	0.967							
5.											

NO.	Pc	Pw	Pwf	Pc ² - Pwf ²	(1) $\frac{Pc^2}{Pc^2 - Pwf^2} =$	(2) $\left[\frac{Pc^2}{Pc^2 - Pwf^2} \right]^n =$
1.	33.6	190.3	36.2	5.1	6.585	6.305
2.	32.5	189.0	35.7	5.6		
3.	31.0	187.1	35.0	6.3		
4.	30.0	185.9	34.6	6.7		
5.						

Pc 203.2 Pc ² 41.3		$AOF = Q \left[\frac{Pc^2}{Pc^2 - Pwf^2} \right]^n = 3653$	
Mcf @ 15.025		Angle of Slope θ 44	
		Slope, n 0.977	

Remarks		
Approved By Commission	Conducted By: LEEROY RICHARDS	Calculated By: MYKOL RENO
		Checked By: PINSON MCWHORTER

