

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

MAY 12 1971

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 5-6-71			
Company Hanagan Petroleum Corporation					Connection Shut in		D. C. C. ARTESIAL DEPT	
Pool Undesignated			Formation Morrow			Unit Catclaw Draw		
Completion Date 5/11/71		Total Depth 10905		Plug Back TD 10855		Elevation 3425 KB		Farm or Lease Name Catclaw Draw Unit
Csg. Size 4 1/2	Wt. 11.60	d 4.000	Set At 10905	Perforations: From 10202 To 10570		Well No. 1-Y		
Tbg. Size 2 3/8	Wt. 4.7	d 1.995	Set At 10109	Perforations: From Open To Ended		Unit F	Sec. 26	Twp. 21S
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 10109		County Eddy		
Producing Thru Tubing		Reservoir Temp. °F 181 @ 10386		Mean Annual Temp. °F		Baro. Press. - P _a 13.2		State New Mexico
L 10386	H 10386	Gg 0.600	% CO ₂	% N ₂	% H ₂ S	Prover 2"	Meter Run	Taps

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI				3459			3459		Packer	
1.	2" x 1/4"			1421		70	1421	70		
2.	2" x 7/32"			1662		72	1662	72		
3.	2" x 3/16"			1901		73	1901	73		
4.	2" x 1/8"			2598		78	2598	78		
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	1.0870		1434.2	0.9905	1.291	1.112	2217
2	0.8393		1675.2	0.9887	1.291	1.126	2021
3	0.6082		1914.2	0.9877	1.291	1.136	1686
4	0.2648		2611.2	0.9831	1.291	1.129	991
5							

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio <u>110</u> Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons <u>58</u> Deg.
2.	BHP Measured with				Specific Gravity Separator Gas <u>.584</u> X X X X X X X X
3.					Specific Gravity Flowing Fluid X X X X X
4.	Amerada RPG-3 Gauge				Critical Pressure <u>671</u> P.S.I.A. <u>671</u> P.S.I.A.
5.					Critical Temperature <u>358</u> R <u>358</u> R

P _f <u>4392.2</u>	P _{f2} <u>19291</u>		
NO.	P _t ²	P _s ²	P _{f2} - P _s ²
1	1950.2	3803	15488
2	2198.2	4832	14459
3	2500.2	6251	13040
4	3347.2	11204	8087
5			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ _____

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$ _____

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$ _____

Absolute Open Flow <u>2800</u> Mcfd @ 15.025	Angle of Slope θ <u>45°</u>	Slope, n <u>1.000</u>
Remarks: _____		
Approved By Commission:	Conducted By: Tefteller, Inc.	Calculated By: F. Tefteller
		Checked By: <i>[Signature]</i>