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. .W MEXICO OIL CONSERVATION COMM. .ION

Form C-122
Revised 9-1-65

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED

NOV - 8 1973

O. C. C.
ARTESIA, OFFICE

Type Test: ☐ Initial ☐ Annual ☒ Special			Test Date: 11-2-73	
Company: Texaco Inc.	Connection: Southern Union			Unit: N
Pool: Catclaw Draw	Formation: Morrow			
Completion Date: 8-17-72	Total Depth: 10645	Plug Back TD: 10607	Elevation: 3327	Farm or Lease Name: E. J. Levers Fed. NCT-1
Csg. Size: 4.5 / Wt.: 11.6 / d: 4.00 / Set At: 10645	Perforations: From 10453 To 10507			Well No.: 1
Tbg. Size: 2-7/8 / Wt.: 6.50 / d: 2.441 / Set At: 10405	Perforations: From To			Unit: N / Sec.: 12 / Twp.: 21S / Rge.: 25E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single Gas		Packer Set At: 10405		County: Eddy
Producing Thru: Tubing	Reservoir Temp. °F: 158 @ 10405	Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2	State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
10405	10405	0.589	0.70	0.20	0.0		6.067	Flange

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					3244	60			72
1.	6 x 2.250	518.5	7.8	65	3161	86			24
2.	6 x 2.250	533.2	54.8	60	2960	94			24
3.	6 x 3.000	533.2	33.6	63	2680	95			24
4.	6 x 3.000	658.0	51.8	65	2176	95			24
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	24.38	64.6	531.7	0.9952	1.303	1.045	2139
2	24.38	173.0	546.4	1.0000	1.303	1.048	5773
3	44.51	135.6	546.4	0.9971	1.303	1.047	8230
4	44.51	186.5	671.2	0.9952	1.303	1.057	11412
5							

NO.	P_r	Temp. °R	T_r	Z
1	0.79	525	1.47	0.915
2	0.81	520	1.45	0.910
3	0.81	523	1.46	0.912
4	0.99	525	1.47	0.892
5				

Gas Liquid Hydrocarbon Ratio 324.7 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons 54.8 Deg.
Specific Gravity Separator Gas 0.589 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX 0.598
Critical Pressure 676 P.S.I.A. 675 P.S.I.A.
Critical Temperature 356 R 358 R

P_c 3257 P_c^2 10609.3

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	10075.5	3182	10127.2	482.2
2	8820.9	3031	9186.9	1422.4
3	7253.3	2818	7939.2	2670.2
4	4792.6	2463	6065.8	4543.6
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.542$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2.006$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 22889$

Absolute Open Flow 22889 Mcfd @ 15.025 | Angle of Slope θ 53.3 | Slope, n 0.74601

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	R. E. Lee	Computer	