

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 10-18-72		OCT 26 1972	
Company Hanagan Petroleum Corporation			Connection Shut-in, waiting on pipeline connection		O. C. C. ARTESIA, OFFICE
Pool Catclaw Draw		Formation Morrow		Unit Catclaw Draw	
Completion Date 10-18-72		Total Depth 10700		Plug Back TD 10681	
Elevation 3304 GL		Farm or Lease Name Catclaw Draw Unit		Well No. 6	
Csg. Size 5 1/2	Wt. 17#	d 4.892	Set At 10700	Perforations: From 10534 To 10621	
Tbg. Size 2 7/8	Wt. 6.5#	d 2.441	Set At 10468	Perforations: From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 10468	
Producing Thru Tubing		Reservoir Temp. °F 174 @ 10400		Mean Annual Temp. °F 70	
Baro. Press. - P _a 13.2		County Fddy		State New Mexico	
L 10578	H 10578	Gg 0.585	% CO ₂	% N ₂	% H ₂ S
Prover Pos. Ck		Meter Run		Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	Positive Choke			3487			3487		Pkr.		
1.	2"	X	8/64	3309		65	3309	65	"		45 Min.
2.	2"	X	10/64	3183		65	3183	65	"		60 Min.
3.	2"	X	13/64	2836		65	2836	65	"		60 Min.
4.	2"	X	16/64	2539		65	2539	65	"		60 Min.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	0.2618		3322.2	0.9952	1.307	1.108	1253
2	0.4173		3196.2	0.9952	1.307	1.113	1931
3	0.7208		2849.2	0.9952	1.307	1.123	3000
4	1.1120		2552.2	0.9952	1.307	1.130	4171
5							

NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	Dry Gas	Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons	None	Deq.
2.	Simplified Supercompressibility tables used.				Specific Gravity Separator Gas	0.585	XXXXXXXXXX
3.					Specific Gravity Flowing Fluid	XXXXXX	
4.					Critical Pressure	675.7	P.S.I.A.
5.					Critical Temperature	353.4	R

P _f 4428.2 P _f ² 19609				
NO.	P _i ²	P _s	P _s ²	P _f ² - P _s ²
1		4225.2	17852	1757
2		4069.2	16558	3051
3		3658.2	13382	6227
4		3309.2	10951	8658
5				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{P_c^2}{P_c^2 - P_w^2}$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$$

Absolute Open Flow	7750	Mcf/d @ 15.025	Angle of Slope @	0.75178	Slope, n	53° 4'
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Remarks: BHP measured with Amerada RPG-3 gauge.

Approved by Commission:	Conducted By: Tefteller, Inc.	Calculated By: F. Tefteller	Checked By:
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