

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-69

RECEIVED

file
22 file
apr

FEB 12 1973

Type Test ☐ Initial ☒ Annual ☒ Special				Test Date 1-25-73		FEB 12 1973	
Company Hanagan Petroleum Corp.				Connection Llano Inc.		O. C. C. ARTESIA, OFFICE	
Pool Catclaw Draw				Formation Morrow		Unit Catclaw Draw	
Completion Date 10-18-72		Total Depth 10700		Plug Back TD 10681		Elevation 3304 GL	
Csq. Size 5 1/2		Wt. 17#		Set At 10700		Perforations: From 10534 To 10621	
Thq. Size 2 7/8		Wt. 6.5		Set At 10468		Perforations: From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 10468		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 174 @ 10400		Mean Annual Temp. °F 70		Baro. Press. - P _a 13.2	
L 10578		H 10578		G _g 0.585		% CO ₂ % N ₂ % H ₂ S	
Prover Meter Run X				Taps			

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI							3118		Packer	
1.	4"	X	2.000	800	2	74	2992	72		
2.	4"	X	2.000	800	7.5	72	2882	72		
3.	4"	X	2.000	830	16	61	2598	72		
4.	4"	X	2.000	840	30	60	2249	72		
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	19.81	40.3	813.2	.9868	1.307	1.061	1092.5
2	19.81	78.1	813.2	.9887	1.307	1.061	2121.2
3	19.81	116.2	843.2	.9990	1.307	1.071	3219.0
4	19.81	160.0	853.2	1.000	1.307	1.071	4436.8
5.							

NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	Dry Gas	Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons	None	Deq.
2.					Specific Gravity Separator Gas	0.585	X X X X X X X X
3.					Specific Gravity Flowing Fluid	X X X X X	
4.					Critical Pressure	675.7	P.S.I.A.
5.					Critical Temperature	353.4	R

P _f 3931.2	P _f ² 15454		
NO.	P _i ²	P _s ²	P _f ² - P _s ²
1.	3775.2	14252	1202
2.	3571.2	12753	2701
3.	3317.2	11004	4450
4.	2926.2	8563	6891
5.			

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} =$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$$

Absolute Open Flow	8,600	Mcf/d @ 15.025	Angle of Slope @ 51° 53'	Slope, n 0.78440
--------------------	-------	----------------	--------------------------	------------------

Remarks: BHP measured with Amerada RPG-3 gauge.

Approved By Commission:	Conducted By: Tefteller, Inc.	Calculated By: F. Tefteller	Checked By:
-------------------------	----------------------------------	--------------------------------	-------------