

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 2-24-73		MAR 5 1973	
Company Inexco Oil Company				Connection <i>not connected</i> Southern Union Gas Co.			O.C.C.	
Pool Catclaw Draw				Formation Morrow			Unit ARTESIA, OFFICE	
Completion Date 2-5-73		Total Depth 11075		Plug Back TD 10995		Elevation 3462 KB		Form or Lease Name Boscowitz
Csg. Size 4 1/2	Wt. 11.6	d 4.000	Set At 11075	Perforations: From 10804 To 10820			Well No. 1	
Tbg. Size 2 7/8	Wt. 6.5	d 2.441	Set At 10590	Perforations: From To			Unit Sec. Twp. Rye. F 30 21S 26E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 10590			County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 179 @ 10500		Mean Annual Temp. °F 70		Baro. Press. - P _a 13.2" Hg		State New Mexico
L 10812	H 10812	Gg 0.626	% CO ₂ 0.75	% N ₂ 0.59	% H ₂ S	Prover Pos. Ck	Meter Run	Taps

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI				3265			3265		Pkr.		
1.	2"	x	8/64"	3139		64	3139	64			60 min.
2.	2"	x	10/64"	3039		67	3039	67			60 min.
3.	2"	x	13/64"	2809		69	2809	69			60 min.
4.	2"	x	16/64"	2347		71	2347	71			60 min.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	0.2618		3152.2	0.9962	1.264	1.147	1191.9
2	0.4173		3052.2	0.9933	1.264	1.144	1829.4
3	0.7208		2822.2	0.9915	1.264	1.153	2939.5
4	1.1120		2360.2	0.9896	1.264	1.160	3808.2
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Dry Gas	Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons		Deg.
2.	Used Simplified				Specific Gravity Separator Gas	XXXXXX	0.626
3.	Supercompressibility Tables				Specific Gravity Flowing Fluid	XXXXX	670
4.					Critical Pressure	P.S.I.A.	P.S.I.A.
5.					Critical Temperature	R	368 R

P _f 4256.2 P _{f2} 18115				$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \text{_____}$ $(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \text{_____}$		
NO.	P _t ²	P _s	P _s ²	P _{f2} ² - P _s ²	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \text{_____}$	
1		4109.2	16886	1229		
2		3984.2	15874	2241		
3		3730.2	13914	4201		
4		3204.2	10267	7848		
5						

Absolute Open Flow 9800 Mcfd @ 15.025		Angle of Slope 53° 33'		Slope, n 0.83974
Remarks: BHP measured with Amerada RPG-3 gauge.				
Approved By Commission:		Conducted By: Tefteller, Inc.		Calculated By: F. Tefteller
Checked By:				