NEW MEXICO OIL CONSERVATION COMMISSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED
JUN 15 1973
O. C. C.
ARTESIA, OFFICE

Type Test: ☒ Initial ☐ Annual ☐ Special				Test Date: 5-22-73	
Company: Texas Oil & Gas Corp.		Connection: None			Unit:
Pool: Carlsbad, South		Formation: Morrow			
Completion Date: 5-22-73	Total Depth: 11,900		Plug Back TD: 11,860	Elevation:	Farm or Lease Name: City of Carlsbad
Csg. Size: 4 1/2" (Liner)	Wt.: 11.6	d: Packer	Set At:	Perforations: From 11312 To 11,444	Well No.: 1
Tbg. Size: 2 3/8	Wt.: 4.6	d: 1.9981	Set At: 11,200	Perforations: From To	Unit: O Sec.: 13 Twp.: 22-S Rge.: 26-E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single			Packer Set At: 11,200		County: Eddy
Producing Thru: Tubing	Reservoir Temp. °F: 190 @ 11,400	Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2		State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
11,200	11,200	.60	1.10	.30	---			

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI				3275			[illegible]				72 hrs
1.	2		1 1/4	Orifice	well	85	2912				60"
2.	2		1 1/4	tester		87	2798				60"
3.	2		1 1/4			87	2659				60"
4.	2		1 1/4			88	2312				60"
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	383		3.5	.9768	1.291	1.0	483
2	491	(orifice well	5.5	.9750	1.291	1.0	618
3	648	tester)	9.0	.9750	1.291	1.0	816
4	915		16.0	.9741	1.291	1.0	1151
5							

NO.	P_t	Temp. °R	T_r	Z
1	4.36	545	1.53	.797
2	4.19	547	1.54	.797
3	4.00	550	1.54	.793
4	3.51	551	1.55	.794
5				

Gas Liquid Hydrocarbon Ratio: Dry Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: Dry Deg.
Specific Gravity Separator Gas: 0.60 XXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 675 P.S.I.A. ____ P.S.I.A.
Critical Temperature: 356 R ____ R

P_c 3273 P_c^2 10,713

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	8266	2943	8661	2052
2	7590	2830	8009	2704
3	6812	2702	7301	3412
4	6260	2369	5612	5101
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.100$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2.100$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2417$

Absolute Open Flow: 2417 Mcfd @ 15.025 | Angle of Slope θ: 45 | Slope, n: 1

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	[signature]	[signature]	