

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

RECEIVED

Copy 451
C-122

Type Test ☐ Initial ☐ Annual ☒ Special					Test Date 10-11-73		OCT 23 1973		
Company Monsanto Company				Connection Transwestern Pipeline Company			O. C. C. ARTESIA, OFFICE		
Pool Burton Flat Strawn				Formation Strawn			Unit V		
Completion Date 3-25-73		Total Depth 11,546		Plug Back TD 11,472		Elevation 3223 DF		Farm or Lease Name Burton Flat, Unit	
Csg. Size 7"	Wt. 26#	d 6.276	Set At 11,546	Perforations: From 10,208 To 10,250			Well No. 3-UT		
Teg. Size 2 3/8 EUE	Wt. 4.7	d 1.995	Set At 9960	Perforations: From To			Unit Sec. Twp. Rge. V 3 21-S 27-E		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual					Packer Set At 9950		County Eddy		
Producing Thru Tubing		Reservoir Temp. °F 151 @ 10,229		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State New Mexico	
L 10,229	H 10,229	Gg .696	% CO ₂ .38	% N ₂ .88	% H ₂ S 0	Prover	Meter Run X	Taps	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
1.	2"	1.125	870	8	71	2942	72				1 Hr
2.	2"	1.125	870	18	75	2713	74				1 Hr
3.	2"	1.125	870	45	76	2357	74				1 Hr
4.	2"	1.125	870	64	78	1992	77				1 Hr
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1.	6.393	84.06	883.2	.9896	.9285	1.102	544
2.	6.393	126.09	883.2	.9859	.9285	1.106	816
3.	6.393	199.36	883.2	.9850	.9285	1.102	1284
4.	6.393	237.75	883.2	.9831	.9285	1.102	1529
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	15017 Mcf/bbl.
1.	1.32	531	1.35	.823	A.P.I. Gravity of Liquid Hydrocarbons	63.6 Deg.
2.	1.32	535	1.36	.818	Specific Gravity Separator Gas	.696 XXXXXXXXX
3.	1.32	536	1.37	.823	Specific Gravity Flowing Fluid	XXXXX
4.	1.32	538	1.37	.823	Critical Pressure	668 P.S.I.A. 664 P.S.I.A.
5.					Critical Temperature	392 °R 441 °R

P _c 3268.2	P _c ² 10681	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{10681}{6587}$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.48922$
NO.	P _w	P _w ²	P _c ² - P _w ²
1.	2955.9	8737	1944
2.	2730.9	7458	3223
3.	2377.2	5651	5030
4.	2023.3	4094	6587
5.			

Absolute Open Flow		2277 Mcfd @ 15.025	Angle of Slope	50.5°	Slope, n	.824
Remarks:						
Approved by Commission:						
Conducted By:		W. T. Hagler		Calculated By:		H. L. Hagler
WEST TEXAS CONSULTING SERVICE, INC.						